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TRANSONIC WIND TUNNEL MEASUREMENTS OF TAILPLANE AND ELEVATOR EFFECTIVENESS OF THE JINDIVIK 203B TARGET AIRCRAFT

by

B. D. FAIRLIE

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B. D/FAIRLIE

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SUMMARY

Measurements of tailplane and elevator effectiveness are reported for a 1/20th scale complete model of the Jindivik target aircraft. The model reflected the Mk.203B version of the full scale aircraft, the major features of which are as follows: short wing with Mk.8 fuel pods (with fins), nominal $+1^{\circ}$ twisted flap, fixed ailerons drooped at $1\frac{1}{4^{\circ}}$: extended chord tailplane with a nominal setting of $-\frac{1}{4^{\circ}}$. The tests included tailplane angles in the range $-2\frac{1}{4^{\circ}}$ to $3\frac{1}{4^{\circ}}$ and elevator angles in the range -15° to 10° for Mach numbers between 0.5 and 0.9. The aircraft is shown to be generally stable throughout the tested ranges, but several small areas of instability are noted. Tailplane and elevator angles to trim are also included and both are shown to increase rapidly for Mach numbers above 0.75.

POSTAL ADDRESS: Chief Superintendent, Aeronautical Research Laboratories, Box 4331, P.O., Melbourne, Victoria, 3001, Australia.

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NOTATION

- a_1 Tailplane effectiveness = $\partial C_{LT}/\partial \alpha_T = \partial C_{LT}/\partial \gamma_T$
- a_2 Elevator effectiveness = $\partial C_{LT}/\partial \eta$
- b Model nominal wingspan = 11.40 in (289.56 mm)
- C_C Cross wind force coefficient = Cross wind force/ $\frac{1}{2}\rho v^2 S$
- C_D Drag force coefficient = Drag force/ $\frac{1}{2}\rho v^2 S$
- C_L Lift force coefficient = Lift force/ $\frac{1}{2}\rho v^2 S$
- C_{LT} Tailplane lift force coefficient = Tailplane lift force/ $\frac{1}{2}\rho v^2 S_T$
- C_X Axial force coefficient = Axial force/ $\frac{1}{2}\rho v^2 S$
- C_{XB} Base force coefficient = $(p_B p)S_B/\frac{1}{2}\rho v^2S$
- C_Y Side force coefficient = Side force/ $\frac{1}{2}\rho v^2 S$
- C_z Normal force coefficient = Normal force/ $\frac{1}{2}\rho v^2 S$
- C_l Rolling moment coefficient = Rolling moment about centre of gravity/ $\frac{1}{2}\rho v^2Sb$
- C_m Pitching moment coefficient = Pitching moment about centre of gravity/ $\frac{1}{2}\rho v^2 Sc$
- C_n Yawing moment coefficient = Yawing moment about centre of gravity/ $\frac{1}{2}\rho v^2Sb$
- c Model wing chord = 2.40 in. (60.96 mm)
- Distance from model centre of gravity to 25% tailplane chord = 5.78 in (146.8 mm)
- M Free stream Mach number
- p Free stream static pressure
- p_B Model base pressure
- R Reynolds number based on model wing chord
- S Model nominal wing area = $27 \cdot 36 \text{ in}^2 (17651 \text{ mm}^2)$
- S_B Model base area = $0.83 \text{ in}^2 (535.5 \text{ mm}^2)$
- S_T Model nominal tailplane area = $5.265 \text{ in}^2 (3396 \text{ mm}^2)$
- V Tail volume ratio = $S_T I/S_C = 0.463$
- v Free stream velocity
- Angle of incidence: the angle between the wind vector and its projection in the chordal plane.
- Alternative angle of incidence: the angle between the model axis and the projection of the wind vector on the model plane of symmetry.
- α_T Tailplane angle of incidence.
- β Angle of sideslip: the angle between the wind vector and its projection on the model plane of symmetry.
- η Elevator angle with respect to tail plane chord.
- $\bar{\eta}$ Elevator angle to trim $(C_m = 0)$

- 7T Tailplane angle with respect to fuselage reference line.
- $\bar{\eta}_T$ Tailplane angle to trim $(C_m = 0)$
- ρ Free stream density.
- φ Model roll angle.

Notes:

- (i) See Figure 1 for sign conventions for forces and moments and attitude angles.
- (ii) The nominal aircraft centre of gravity was taken to be located at 0·2 c and 0·1125 in.
 (2·8575 mm) (model scale) below the fuselage reference line.
- (iii) Since the full scale aircraft and the model were both manufactured before the introduction of SI units, all dimensions have been expressed in feet and inches, with the equivalent SI unit following in brackets where appropriate.

1. INTRODUCTION

In 1976 a decision was made to update the data available from wind tunnel tests covering the high speed flight envelope of the Jindivik target aircraft. This update became necessary because of the considerable changes to the basic aircraft configuration, which had occurred since the last major series of tests in the period 1956 to 1965.¹⁻⁹ These included changes to control surfaces, pods and pod fins, and to payloads carried. A new test programme was therefore implemented on an existing 1/20th scale complete model of the Jindivik which had been modified to reflect the current full scale aircraft configuration. These tests 10 covered the lateral and longitudinal stability of the aircraft and the effect on stability of various combinations of Tonic towed targets and their mounting beams.

The present tests complement and extend the 1976 tests, being concerned with tailplane and elevator effectiveness. The only previous similar tests were performed in 1962^{2,3} and were made using a half model of the aircraft. Since that time however, the tailplane and elevator chords have been increased so that none of the available data is pertinent to the current aircraft configuration.

The present tests were conducted in the transonic wind tunnel of the Aeronautical Research Laboratories during July and August 1979.

2. TEST DETAILS

2.1 Model

The model used for these tests was a 1/20th scale complete metal model of the Jindivik aircraft modified to reflect the Mk.203B version of the full-scale aircraft. The major features of the configuration are as follows: short wing with Mk.8 fuel pods (with fins), nominal $+1^{\circ}$ twisted flap, fixed aileron drooped at $+1\frac{1}{2}^{\circ}$. No intake ducting was represented and an unfaired landing skid was represented in the stowed position. The major dimensions of the model and full-scale aircraft are given in Table 1. A sketch of the aircraft is presented in Figure 2 and a photograph of the model in Figure 3.

Due to the small size of the model, the elevator could not be hinged and changes to tailplane angle (ηT) and elevator angle (η) were obtained by removing the tailplane from its mounting block and remounting at the desired angle. Several tailplanes were available and the required elevator angles were obtained by bending at the elevator hinge line.

Owing to the low Reynolds number of the tests (approximately 0.45×10^6), boundary layer transition was fixed on all windswept surfaces by bands of distributed roughness. These roughness bands were placed on the upper and lower surfaces of the wing and tailplane, on both sides of the fin and pod fins, and on the pods and fuselage. They consisted of approximately 3 mm wide bands of carborundum particles, with a particle diameter of 0.15 mm and a coverage of $10-20^{\circ}_{0}$.

2.2 Wind Tunnel

The tests were conducted in the transonic wind tunnel of these laboratories. The nominal dimensions of the test section are 0.81 m by 0.53 m. For these tests, all test section walls were longitudinally slotted (see Fig. 4) with an open area ratio at the model location of 10.5%.

The maximum frontal cross-sectional area of the model at zero incidence was 5.36 in.² (3458 mm²) giving a blockage ratio of 0.81° , and since the ranges of angle of incidence and Mach number of the tests were limited, no tunnel interference corrections were applied to the results.

Mach number and dynamic pressure were derived from measurements of the static pressure in the plenum chamber surrounding the test section and of the static pressure in the contraction entry, assuming these to be the static and total pressures respectively of the test section flow.

2.3 Test Programme

Six-component force and moment coefficients were measured for a range of Mach number $0.50 \le M \le 0.90$ in eight steps. The tests covered seven tailplane angles in the range $-2\frac{1}{2}^{\circ} \le \eta_T \le 3\frac{1}{2}^{\circ}$ (for $-3^{\circ} \le \alpha \le 7^{\circ}$, $\beta = 0^{\circ}$, $\eta = 0^{\circ}$) and six elevator angles in the range $-15^{\circ} \le \eta \le 10^{\circ}$ (for $0^{\circ} \le \alpha \le 6^{\circ}$, $\beta = 0$, $\eta_T = \frac{1}{2}^{\circ}$). In addition tests were conducted with the tailplane removed for $-3^{\circ} \le \alpha \le 7^{\circ}$ ($\beta = 0^{\circ}$) at Mach numbers of 0.5, 0.8 and 0.9. Throughout the tests, model altitude was corrected for sting and balance deflection under load.

Test results are tabulated in Tables 2, 3 and 4. Tailplane and elevator angles referred to in these tabulations and elsewhere in this report are nominal angles: the corresponding measured angles are given below.

Nom	inal	Meas	ured	Nom	inal	Measu	ıred
ητ	η	ητ	η	η	ητ	η	ητ
	0 °	-2·52°	0.00°	-15°	j°	-17·45°	0·50°
-1 <u>\$</u> °	0 °	-1·42°	0.00°	-10°	į°	-10·25°	0 · 50°
- ½°	0°	_0.50°	0.00°	-5°	1º	-4·50°	ე∙50°
į٠	0 °	0 · 50°	0.00°	0 °	į°	0.00°	0·51°
l ½°	0 °	1 · 78°	0.00°	5°	į°	5 · 50°	0·52°
2½°	0 °	2·68°	0.00°	10°	į°	10·25°	0·44°
3į°	0 °	3.90°	0.00°		•	,	

Measurement accuracy for the above angles was $\pm 0.02^{\circ}$ for η_T and $\pm 0.05^{\circ}$ for η . For all tests, the Reynolds number (based on wing chord) was kept approximately constant at $0.45\pm0.03\times10^{6}$ by varying tunnel pressure.

3. RESULTS AND DISCUSSION

The data are plotted in the form of lift coefficient versus angle of incidence in Figure 5 for the various nominal tailplane angles, in Figure 6 for the various nominal elevator angles and in Figure 7 for the case with the tailplane removed. From Figures 5 and 6 it is seen that as expected the effect of variations of tailplane and elevator angles on the overall lift coefficient is small.

In Figure 8 pitching moment coefficient is plotted against angle of incidence for the various tailplane angles. For the current standard tailplane setting $(\eta_T = -\frac{1}{2}^{\circ}, \eta = 0^{\circ})$ the aircraft is seen to be stable for all Mach numbers tested for angles of incidence less than about 7°, apart from an area around $\alpha = 6^{\circ}$ for M = 0.80. The aircraft is also seen to be stable at all other values of tailplane angle tested except for a region of instability at Mach numbers greater than 0.86 and angles of incidence greater than 7° for a tailplane angle of $3\frac{1}{2}^{\circ}$.

The same variables are plotted in Figure 9 for the various elevator angles. Once again the curves show general stability throughout the tested range except at an elevator angle of 10° where instability occurs for Mach numbers greater than 0.80 and angles of incidence greater than about 2° . This unstable area extends into the data for an elevator angle of 5° but is limited to higher Mach numbers and angles of incidence.

Figure 10 presents the same variables for the case with the tailplane removed. As found in previous tests¹⁰, the aircraft without tailplane is generally unstable, but with an area of stability at M = 0.9 at low incidence.

The variation of pitching moment coefficient with tailplane angle is presented in Figure 11 for constant angles of incidence ($\alpha = 0^{\circ}$, 2° , 4°). The curves are seen to be generally linear

except at Mach numbers greater than 0.84 for positive values of η_T . There is also evidence of tailplane stalling at Mach numbers above 0.86 for $\alpha = 4^{\circ}$.

Figure 12 presents the variation of pitching moment coefficient with elevator angle. Once again the curves are generally linear at least for small elevator deflections ($-10^{\circ} < \eta < 5^{\circ}$). Tailplane stalling is evident for Mach number greater than 0·7 at large negative elevator angles ($\eta \le -10^{\circ}$) for all incidences, and becoming increasingly evident at higher Mach numbers and positive elevator angles as incidence increases.

From Figures 11 and 12, values of tailplane angle and elevator angle to trim were obtained from the intersection of the curves with the horizontal axis $(C_m = 0)$. These values are plotted against Mach number in Figures 13 and 14, for different values of incidence. It may be seen that as the Mach number approaches 0.8 the angle required for both elevator and tailplane to trim out the pitching moment increases rapidly. However for angles of incidence up to 4° , an η_T of -4° is sufficient to trim out the pitching moment up to a Mach number of 0.9, or for $\eta_T = \frac{1}{2}^\circ$, an elevator angle of -9° is sufficient.

Values of tailplane and elevator effectiveness have also been obtained from Figures 11 and 12 from the relationships:

$$a_{1} = \frac{\partial C_{LT}}{\partial \alpha_{T}} = \frac{\partial C_{LT}}{\partial \eta_{T}}$$
$$= \frac{\partial C_{m}}{\partial \eta_{T}} \frac{1}{V}$$

and

$$a_2 = \frac{\partial C_{LT}}{\partial \eta}$$
$$= \frac{\partial C_m}{\partial \eta} \frac{1}{V}$$

where V is the tail volume ratio $(S_T l/S_C)$.

In both cases, the slopes of the pitching moment curves have been obtained from the linear portions of the curves of Figures 11 and 12. Values of tailplane and elevator effectiveness are plotted against Mach number in Figures 15 and 16.

4. CONCLUSIONS

Transonic wind tunnel tests have been carried out on a 1/20th scale complete model Jindivik 203B to determine tailplane and elevator effectiveness. The tests covered tailplane angles between $-2\frac{1}{2}^{\circ}$ and $3\frac{1}{2}^{\circ}$ and elevator angles between -15° and 10° for Mach numbers from 0.5 to 0.9.

The tests indicates that the aircraft is generally stable throughout the range of tailplane and elevator angles tested, although several small areas of instability were discovered and have been noted.

Curves of tailplane and elevator effectiveness and tailplane and elevator angles to trim have been extracted from the data. The latter curves indicate that both tailplane and elevator angle to trim increase rapidly above a Mach number of 0.75. The present elevator size should however be sufficient to trim the aircraft for Mach numbers up to 0.9.

REFERENCES

1. Bennett, A. S. The effect of externally mounted F. H. Sources on the longitudinal stability and drag of a Jiniivik target aircraft. Aeronautical Research Laboratories, Tech. Note, Aero. 183, 1960. 2. O'Brien, L. F. Lift, pitching moment and drag measurements on a half model Jindivik target aircraft. Part I-4° Flap. Aeronautical Research Laboratories, Tech. Note, Aero. 192, 1962. 3. O'Brien, L. F. Lift, pitching moment and drag measurements on a half model Jindivik target aircraft. Part II-20° Flap. Aeronautical Research Laboratories, Tech. Note, Aero. 193, 1962. 4. Bennett, A. S. The effect of rocket fuel pods on the longitudinal stability and drag of Jindivik target aircraft. Aeronautical Research Laboratories, Tech. Note, Aero. 199, 1962. 5. Bennett, A. S. Transonic wind tunnel measurements of the longitudinal and lateral stability of a 1/20th scale Jindivik 11B/III target aircraft. Aeronautical Research Laboratories, Tech. Note, Aero. 195, 1962. 6. O'Brien, L. F. Longitudinal characteristics of an extended tapered wing version of the Jindivik target aircraft. Aeronautical Research Laboratories, Tech. Note, Aero. 253, 1965. 7. Bennett, A. S. Effect of an air brake on the high speed longitudinal stability and drag Aeronautical Research Laboratories, Tech. Note, Aero. 255, 1966. 8. O'Brien, L. F. Force measurements on the short span Jindivik aircraft fitted with Aeronautical Research Laboratories, Tech. Note, Aero. 264, 1966. 9. O'Brien, L. F. Effect of MK VII Ampor pod end shape on Jindivik. Aeronautical Research Laboratories, Tech. Note, Aero. 265, 1966. 10. Fairlie, B. D. Transonic Wind tunnel tests on the Jindivik 203B target aircraft. Aeronautical Research Laboratories, Tech. Note, Aero. 369, 1977.

TABLE 1

Main Dimensions of Model and Full Scale Aircraft

	Model Scale	Full Scale
(1) Wing		;
Chord	2·40 in.	48 · 00 in.
Span (nominal)	11 · 40 in.	228 · 00 in.
To centreline of pods	11 · 82 in.	236 · 48 in.
Gross wing area	27 · 36 in. ²	76 · 0 ft.2
Wing section	NACA 64-10	6 (modified)
Aspect ratio	4.	•
Taper ratio	1.0	0
Leading edge sweep		o°
Trailing edge sweep	}	0°
Dihedral	2.	5°
Incidence relative to F.R.L.	1.	
(2) Flaps	•	1
Chord	0.60 in.	12·00 in.
Span (per side)	3 · 45 in.	68·95 in.
Area (per side)	2·07 in. ²	827 · 4 in.
Distance from inboard end to aircraft datum	0·79 in.	15·75 in.
Neutral (Inboard	+	,
Setting Outboard	1	0°
Nominal setting	+	_
(3) Ailerons	1	1
Chord	0.60 in.	12 · 00 in.
Span (per side)	1 · 35 in.	27 · 00 in.
Area (per side)	0.81 in.2	324 · 0 in.
Distance from inboard end to aircraft datum	4·25 in.	84·96 in.
Neutral setting		04 >0 III.
(4) Mk.8 Pods		
Overall length	7 · 22 in.	144 · 33 in.
Diameter	0.625 in.	12 · 50 in.
Distance from pod centreline to F.R.L.	5.91 in.	118 · 24 in.
Distance from pod nose to 25% wing chord	3 · 70 in.	74·09 in.
(5) Pod Fins	3 /0 111.	/ 7 'U > ill.
1.7	6 · 25 in.	125 · 00 in.
Distance from pod nose to fin trailing edge Root chord	1 · 20 in.	24·00 in.
Tip chord	0.60 in.	12.00 in.
•	1	12.00 in. 18.25 in.
Maximum height above pod centreline	0.91 in.	
Angle between fin and F.R.L.	-	5° \\ (1:6-4\
Aerofoil section	NACA 64-00	o (modined)
(6) Tailplane	1 25.	22.00:
Chord	1 · 35 in.	27·00 in.
Span	3 · 90 in.	78 · 00 in.
Gross area	5 · 265 in. ²	2106 · 0 in.
Aspect ratio	2.	
Taper ratio	1	
Sweep at quarter chord]	0°
Incidence relative to F.R.L.	_j°	-0°27′
Aerofoil section	NACA	64-006

TABLE 1 (Continued)

Main Dimensions of Model and Full Scale Aircraft

	Model Scale	Full Scale
(7) Elevators		
Chord	0·45 in.	9·00 in.
Span (per side)	1 · 63 in.	32·64 in.
Area (per side)	0 · 73 in.2	293 · 4 in. ²
Distance from inboard end to F.R.L.	0·28 in.	5·55 in.
(8) Fin		
Maximum height above F.R.L.	2·64 in.	52 · 80 in.
Gross area above tailplane chord	2·35 in.2	938 · 9 in. ²
Sweep back of leading edge	14	j c
Swwep back of trailing edge	(O _c
Tip chord	1 · 20 in.	24 · 00 in.
Root chord	1 · 60 in.	32 · 00 in.
Aerofoil section	NACA 64-00	6 (modified)
(9) Fuselage		
Overall length (excluding pitot probe)	13 · 99 in.	279 · 75 in.
Maximum height excluding skid beam	1 · 90 in.	38 · 04 in.
Maximum width	1 · 65 in.	33 · 00 in.
Distance of 25% wing chord aft of STN 'O'	6·61 in.	132 · 25 in.
Distance of 25° wing chord below F.R.L.	0·41 in.	8 · 25 in.
Distance of 25% tailplane chord aft of STN 'O'	12·27 in.	245 · 45 in.
Distance of 25° v tailplane chord above F.R.L.	0·86 in.	17·24 in.
Distance of fin trailing edge aft of STN 'O'	13·17 in.	263 · 37 in.

The following notation refers to the computer generated data listings in Tables 2-4. Where appropriate, the corresponding notation from the main body of the note is also included

Table 2	Main Body	Explanation
Notation	Notation	
SER		Serial number
REYN	R	Reynold's number
MACH	М	Free stream Mach number
INCID.	α	Angle of incidence
LIFT.	C_L	Lift coefficient
PITCH	C_m	Pitching moment coefficient
DRAG	C_D	Drag force coefficient
NORMAL	Cz	Normal force coefficient
AXIAL	C_{X}	Axial force coefficient
CLSQ.	C_{L^2}	Lift coefficient squared
BASE	C_{XB}	Base force coefficient
AINC	α_1	Alternative angle of incidence
SLIP	β	Angle of sideslip
CROSS	$C_{\rm C}$	Cross wind force coefficient
YAW M.	C_n	Yawing moment coefficient
ROLL M.	C_l	Rolling moment coefficient
RANG	φ	Roll angle
SIDE F	Cy	Side force coefficient

INDEX TO TABLES 2, 3 and 4

Table No.	ητ	η	α
2A	-2½°	0°	-3° to 7°
2 B	-1½°	0°	-3° to 7°
2C	- <u>1</u> °	0 °	-3° to 7°
2D	<u>,</u> °	0 °	-3° to 7°
2E	١½°	0 °	-3° to 7°
2F	2 <u>1</u> °	0°	-3° to 7°
2G	3½°	0 °	-3° to 7°
3A	į°	—15°	0° to 6°
3B	ؠۣٙٞ٥	10°	0° to 6°
3C	į°	−5°	0° to 6°
3D	į°	0°	-3° to 7°
3E	ؠۣٙٙ	5°	0° to 6°
3F	ڼ۰	10°	0° to 6°
4	Tailpla	ne Off	-3° to 7°
	•		

TABLE 2(A) CLERK A)RCRAFT ETA = 0°ETA(T) = -2 1/2°

								ETA = G	ETR(T)	-2 1/2							
REVR	t. HRCH.	THE	D. LIFT	<u>.</u>	I TCH.	DRAG	KORHAL	AX 1 AL.	CL SQ.	BRSE.	AIKC.	St. 1P.	CROSS.	E E	ROLL M	RANG.	SIDE
44444	49 0. 900 47 0. 900 48 0. 901 49 0. 901 49 0. 901	98. 98. 98. 98.	45 0.84 41 0.76 89 0.73 89 0.73	434 -0 1119 -0 588 -0 318 -0	0.0769 0.0738 0.0674 0.0611	0, 1669 0, 1541 0, 1541 0, 1593 0, 1593	-0, 8600 -0, 8247 -0, 7799 -0, 7413	-0.0538 -0.0527 -0.0522 -0.0514	0.7147 0.5592 0.5910 0.5314 0.4788	0.0024 0.0027 0.0027 0.0027 0.0027	0.50 0.30 0.30 0.30 0.30 0.30 0.30 0.30	80 80 80 80 80 80 80 80 80 80 80 80 80 8	-0.0044 -0.0044 -0.0044	-0.0009 -0.0010 -0.0010 -0.0009	-0.0005 -0.0006 -0.0044 -0.0008	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	00000
4444	49 (1. 900 49 (1. 900 49 (1. 900 49 (1. 901 49 (1. 901	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 0. 541 7 0. 248 7 0. 248 8 0. 030 0 0 000 0 0 000 0 0 000 0 0 000 0 0 000 0 0 000 0 0 0 000 0 0 0 000 0 0 0 0	119 - 0. 187 - 0. 304 - 0. 573 0.	. 0283 . 0283 . 0100 . 0224 . 0708	0, 1002 0, 0847 0, 0611 0, 0510 0, 0616	-0.6178 -0.5228 -0.2959 -0.0296	.0.0515 .0.0527 .0.0531 .0.0496	0. 3689 0. 0689 0. 0867 0. 0009 0. 0713	0, 0021 0, 0021 0, 0020 0, 0019 0, 0016	04. 34 03. 29 04. 47 00. 96	20, 00 20, 00 20, 00 20, 01 20, 01	-0.0044 -0.0024 -0.0006 0.0014 0.0030	-0.0007 -0.0005 0.0004 0.0006	0.0004 0.0010 0.0015 0.0016	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
00000 00000	52 (- 880 53 (- 880 53 (- 881 55 (- 861 55 (- 861	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	94 0 84 0 84 0 95 0 95 0 95 0 95 0 95 0 95 0 95 0 9	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	. 0276 . 0633 . 0557 . 0469	0, 1572 0, 1486 0, 1378 0, 1229 0, 1332	-0.8267 -0.8171 -0.7786 -0.7351 -0.6968	-0.0484 -0.0488 -0.0470 -0.0488 -0.0488	0, 6609 0, 6478 0, 5900 0, 5274 0, 4748	0.0019 0.0018 0.0020 0.0020 0.0020	06. 94 06. 42 05. 90 05. 39	(60. 91 (60. 92 (70. 98 (70. 98 (70. 98	-0.0050 -0.0051 -0.0043 -0.0044 -0.0031	-0.0004 -0.0009 -0.0004 -0.0009	0. 0017 -0. 0003 -0. 0010 -0. 0010	180.0 1879.9 1879.9 1879.9	00000
00000 64444 6666	53 (). 880 53 (). 880 55 (). 861 53 (). 881 53 (). 881	9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	36 0.613 20 0.32 20 0.34 34 0.036 10 -0.26	240 -0 173 -0 173 -0 244 0	. 0214 . 0104 . 0102 . 0302	0.0944 0.0576 0.0576 0.0457 0.0576	-0.6167 -0.3278 -0.3185 -0.0538	10.04% 10.04% 10.04% 10.04% 10.04%	0, 3735 0, 2745 0, 1000 0, 0029 0, 0689	0.000 0.000	04.00 03.00 03.00 03.00 03.00	30.00 30.00 30.01 30.01 30.01	-0.0033 -0.0033 -0.0003 0.0011	-0.0011 -0.0002 0.0002 0.0003	0.0002 0.0013 0.0015 0.0017	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	66666
00000	57 0. 862 57 0. 862 57 0. 860 55 0. 859 57 0. 859	2.30 4.3.30 4.0.40	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	. 0346 . 0432 . 0438 . 0361	0.1500 0.1420 0.1420 0.1100 0.1100	-0, 8102 -0, 8055 -0, 7421 -0, 7443	.0, 0433 .0, 0433 .0, 0445 .0, 0405	0.6336 0.3363 0.3463 0.4464	0.0018 0.0021 0.0021 0.0018	06.95 05.95 05.98 05.98	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-0.0050 -0.0063 -0.0044 -0.0044	-0.0011 -0.0011 -0.0010 -0.0009	0. 0033 -0. 0003 -0. 0004 -0. 0004	180.0 180.0 1739.0 1799.9	
00000	55 0. 059 57 0. 860 58 0. 859 55 0. 860	0.40 0.40 0.40 0.40	00000 00000	6200 3334 3334 0.033 2479 0.033 0.033	. 0044 . 0414 . 0414 . 0629	0.0899 0.0746 0.0529 0.0428	-0.523 -0.3366 -0.3305 -0.0526	-0. 0416 -0. 0416 -0. 0444 -0. 0444	0, 3862 0, 19862 0, 1983 0, 0027 0, 0613	0.0020 0.0020 0.0019 0.0018	04. 37 03. 33 04. 22 -00. 93	20.02 20.03 20.03 20.03 20.03	-0.0044 -0.0023 -0.0003 -0.0003 0.0009	-0.0002 0.0002 0.0003 0.0003	0.0012 0.0012 0.0016 0.0016	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	00000
4444	ddddd d Ombmm	98 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		11111	066 044 042 027 016	44444	200 200 200 200 200 200 200 200 200 200		20000 20000	000 200					စ်စ်စ်စုံစ်	2222	
1.	53 O. 841	Š	78 O. 63	0 6259	0. 0015	0. 0864	-0. 6374	-0.035 8	0. 4000	0. 0019	04. 38	90.00	-0. 0033	-0. 000 6	990.0		3

TRBLE 2(4) CLERN HIRCRAFT ETR # 0°ETR(T) # -2 1/2°

SIDE F	0. 0002 0. 0003 0. 0002 0. 0022 0. 0041	0. 0023 0. 0023 0. 0023 0. 0030	0.00010 0.00014 0.0014	0. 0012 0. 0012 0. 0010 0. 0010	0.0004 0.0002 0.0002 0.0012	0. 0011 0. 00013 0. 00012 0. 0012	0.0000000000000000000000000000000000000
RANG.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1180.0 1180.0 1180.0 1180.0	180.0 180.0 180.0	1 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1180 1480 1480 1890 0	
ROLL N	0.0012 0.0017 0.0015 0.0017	0. 0027 0. 0036 0. 0024 0. 0007 0. 0011	0.0022 0.0016 0.0015 0.0017 0.0030	0.0033 0.0033 0.0033 0.0033	0.0022 0.0016 0.0015 0.0018	0.0041 0.0041 0.0032 0.0032	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
NE NE N	0.0004 0.0010 0.0002 0.0003	-0. 0006 -0. 0007 -0. 0004 -0. 0008	-0.0001 0.0003 0.0002 0.0002	-0. 0001 0. 0001 0. 0003	0.0003 0.00000 0.00000 0.00000	0.0000 0.0000 0.0000 0.0000 0.0000	000000000000000000000000000000000000000
CROSS.	0.00023 0.0003 0.0003	0.00324 -0.0024 -0.0034	-0. 0013 -0. 0013 -0. 0013 -0. 0013	0.0023 0.0003 0.0000 0.0011	-0.0003 -0.0013 -0.0001 -0.0014	-0.0014 -0.0014 -0.0003 -0.0013	000000000000000000000000000000000000000
gh. 19.	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0000	00.00 00.00 00.00 00.00 00.00	00.00 00.00 00.00 00.00 00.00 00.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	00000000000000000000000000000000000000
3 XC	03. 23 00. 23 07. 63 07. 63	06.20 06.20 05.24 05.44 05.44	03. 37 04. 22 -00. 93 -03. 07	06.93 06.93 05.93 04.43	03. 34 04. 20 07. 98 07. 98	06.90 06.90 05.00 04.80 04.80	83.20 83.20 84.20 85.20 85.20 87.20
BASE.	0, 0058 0, 0058 0, 0053 0, 0052 0, 0052	0.0047 0.0047 0.0046 0.0047 0.0047	0.0017 0.0057 0.0054 0.0054 0.0058	0.0014 0.0016 0.0016 0.0017 0.0017	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0014 0.0014 0.0014 0.0016	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
E 18(1) #	0, 3022 0, 1062 0, 0020 0, 0360 0, 6529	0, 6138 0, 5738 0, 5738 0, 5738 0, 7368 0, 4868	0, 3440 0, 0886 0, 0044 0, 0484 0, 6417	0, 628 0, 358 0, 358 0, 355 0, 455 0, 455 0, 455	0, 2687 0, 0748 0, 0010 0, 0424 0, 6083	0. 5818 0. 5818 0. 5385 0. 4823 0. 4616	0.03374 0.0006 0.0007 0.0007 0.0007 0.0007 0.0007
RXIAL.	-0. 0374 -0. 0411 -0. 0327 -0. 0327	-0, 0335 -0, 0280 -0, 0280 -0, 0271	-0. 0277 -0. 0359 -0. 0365 -0. 0303	-0.0247 -0.0230 -0.0223 -0.0223	-0, 0237 -0, 0336 -0, 0325 -0, 0321	-0. 0203 -0. 0170 -0. 0156 -0. 0149	-0.0231 -0.0343 -0.0374 -0.0314 -0.0200
RORHAL	-0. 3271 -0. 0433 -0. 0433 -0. 2389	-0. 7950 -0. 7670 -0. 7399 -0. 7406	-0. 5606 -0. 2969 -0. 0369 -0. 8223 -0. 6117	-0, 8019 -0, 7748 -0, 7212 -0, 6472	-0. 5210 -0. 2747 -0. 0321 -0. 2084 -0. 7901	-0.7902 -0.7698 -0.7896 -0.6996	0.000 0 4.0000 0 4.0000 0 4.0000 0 4.0000 0 4.0000 0
DRAG	0. 0711 0. 0413 0. 0413 0. 1407	0.1306 0.1180 0.1061 0.0989	0. 0624 0. 0433 0. 0391 0. 0432	0.1227 0.1112 0.1014 0.0893	0.0555 0.0429 0.0443	0. 1045 0. 0933 0. 0833 0. 0683	0.000 0.000
P I TCH.	0. 0173 0. 0371 0. 0516 0. 0613 -0. 0493	-0.0392 -0.0494 0.0467 0.0046	0.0527 0.0527 0.0577 0.0652 0.052	-0.0165 -0.0037 0.0038 0.0290 0.0318	0.0545 0.0546 0.0646 0.0743	-0.0027 0.0244 0.0232 0.0393	0.0545 0.0545 0.0545 0.05424 0.0000
LIFT.	0. 3260 0. 3260 0. 0459 0. 8089	0.7849 0.7593 0.7327 0.7327 0.6607	0. 5576 0. 2980 0. 0394 -0. 2204 0. 8011	0.7671 0.7671 0.7446 0.7182	0. 5185 0. 2737 0. 0327 -0. 2064 0. 7800	0. 7628 0. 7338 0. 6946 0. 6946	0.000.000.000.000.000.000.000.000.000.
JHCJD.	03. 35 04. 23 -00. 93 -03. 09	26.00 26.00	03. 00 03. 00 03. 00	06.93 05.93 05.43 04.43 04.43	03.34 01.20 -00.93 -03.06	06. 90 05. 40 05. 80 04. 80 04	03.29 00.17 00.34 07.29 86.79 87.88 87.88
. HACH	52 0. 840 57 0. 839 57 0. 839 53 0. 840 53 0. 800	2 C 2 S B C 2	5 0. 799 5 0. 800 5 0. 800 5 0. 800 5 0. 789	2 0 749 0 750 0 750 0 751 0 751 0 751	0.749 0.749 0.730 0.730 0.730 0.730	9 0. 700 9 0. 700 9 0. 700 9 0. 700 9 0. 700	8888 4 4 6666 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
SER REVN	045 045 047 047 047 043 043 043 043 043 043 043 043 043 043	052 0.46 053 0.46 054 0.46 055 0.46	00000	064 0.46 063 0.46 065 0.46 067 0.46 068 0.46	059 0.46 070 0.46 071 0.46 072 0.46	076 0.44 077 0.44 078 0.44 079 0.44	0662 0 44 0672 0 44 0673 0 44 0673 0 44
••							

TABLE 2(A)
(CLEAN A)RCRAFT
FIRE R'ETR(1) = -2 5/

	SIDE F	0.0025 0.0017 0.0009 0.0009	0. 0004 0. 0006 0. 0016
	RAME.	11800 0 11800	100.0 -0.0 100.0 -0.0 100.0 -0.0
	ROLL M	0.0022 0.0024 0.0024 0.0026	0.0017 0.0017 0.0020
	× 34.	000000000000000000000000000000000000000	0. 0004 0. 0001 0. 0002
	CROSS	-0.0023 -0.0023 -0.0018 -0.0010	0.0000 0.00005 0.0045
	91.1P.	100 00 100 00 100 00 100 00 100 00	-00 01 -00 01 -00 01
	A 1 HC	06.22 005.26 04.22 04.22	01. 11 -00. 96 -03. 03
-2 1/2	BRSE.	0.0018 0.0018 0.0020 0.0018 0.0018	0.0017 0.0015 0.0013
TR(T) =	CL SQ.	0, 4815 0, 4229 0, 3666 0, 2636 0, 1765	0, 0504 0, 0004 0, 0322
ETR = 6"ETR(1) = -2 1/2	RX JAL.	-0.0408 -0.0408 -0.0418 -0.0467 -0.0224	
_	HORHAL AXTAL.	-0.6997 -0.6531 -0.3165 -0.3165	-0.2255 -0.0218 0.1817
	DRAG	0.0891 0.0781 0.0695 0.0564	0, 03 84 0, 03 63 0, 04 01
	PITCH.	0. 0381 0. 0381 0. 0394 0. 0429 0. 0459	
	LIFT.	0.6940 0.6504 0.6035 0.5136 0.4202	0, 2247 0, 0223 -0, 1799
	THETO LIFT.	90 90 90 90 90 90 90 90 90 90 90 90 90 9	01, 11 0, 2247 -00, 96 0, 0223 -03, 03 -0, 1799
	HBCH.	0. 301 0. 501 0. 300 0. 301	0. 500 0. 499 0. 499
	SER REVN. HACH.	089 0, 444 0, 303 090 0, 444 0, 499 091 0, 444 0, 500 092 0, 444 0, 501	094 0, 444 0, 500 095 0, 444 0, 699 096 0, 444 0, 699

THBLE 2(B) CLERN H)RCRAFT TA = 0 ETA(T) = -1 5/2

ж ы		REVE	HPCH.	1401	ند	1FT.	PIT	TCH.	PR 36	HORMAL	<u>.</u> ₹	RX FR.		# CT)# CL SQ.	-1 N		Š	St.1P.	CROSS		Y R R	ROLL	RAHEG	S)	2	b.
10 10 10 10 10 10 10 10 10 10 10 10 10 1		8 8 8 8 8 8 8 8 8 8 8 8	888 C C C C C C C C C C C C C C C C C C	23333	4 2 4 2 W	8495 8472 7774 7420 7038	96699	0000 0000 0000 0000 0000 0000 0000	0 1567 0 1567 0 1568 0 1588 0 1588	00000	8442 : 7800 - 7800 - 7813 : 7119 : 7119 : 7119	0.034	400 000	6677 6677 6038 5505	0. 0024 0. 0024 0. 0024 0. 0024	5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 % 9 8 %	65558 82222	0.0001	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0017 0017 0014 0012	-0.0009 -0.0009 -0.0018 -0.0012	****		5100	X2222
20 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0000	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2 2 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	25.98.5	22.52.52.52.52.52.52.52.52.52.52.52.52.5	6233 5284 3066 0361 2636	99900	0659 0543 0315 0020	0.1003 0.082 0.0597 0.0506	96999	6293 : 5323 : 2070 : 0354 : 2664 : 2664	55555 55555	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2790 0938 0038 0048	0.0020 0.0020 0.0019 0.0018	20200	* * * * * * * * * * * * * * * * * * *	30 03 30 03 30 03 30 03 30 03	0.0034	20000 27778	0017 0023 0026 0030	0.0001 0.0007 0.0009 0.0040	1 1 1 1 1		000 X 4 4 000 X	22112
20 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	66666	454 454 454 454 754	C	5 5 5 8 8 5 5 5 8 8	2 2 4 5 7 2 2 2 2 2 2	8097 8093 7763 7374 6998	9999	0177 0779 0779 0700 0703	0. 1549 0. 1354 0. 1354 0. 1229 0. 1229	-0. 823 -0. 7823 -0. 786 -0. 746	2000		2	6455 6555 6556 6556 6556 6556 6556 6556	0.0020 0.0020 0.0020 0.0020 0.0021	25522 25522	\$2.78%	6 6 6 6 6 2 2 2 2 2	-0.0042 -0.0004 -0.0003 1.0.0043	# # # # # # # # # # # # # # # # # # #	0012 0014 0014 0014	0.0018 -0.0003 -0.0012 -0.0012 -0.0008			00011	38835
900 800 800 800 800 800 800 800	00000	457	C	22252	# # # # # # # # # # # # # # # # # # #	5221 5353 3272 0590	99999	0470 0360 0159 0466	0.0927 0.0724 0.0554 0.0526	96.000	6274 5389 3284 0584	ರರ್ಥರ	0 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2863 2863 1. 1070 1. 0034	0.0024 0.0024 0.0025 0.0025 0.0025	#655E	78583	20 00 00 00 00 00 00 00 00 00 00 00 00 00	60000	00020 0020 0042 0043 0065	0017 0020 0020 0030	-0.0003 0.0007 0.0009 0.0012 0.0011	7 9 9 9 9	0000	00000	92467
440 440 440 440 640		£ £ 5 £ £	0. 339 0. 350 0. 360 0. 360 0. 360	25.588	# # # # # # # # # # # # # # # # # # #		0 0 0 0 0	0697 0698 0605 0519	0. 1499 0. 1384 0. 1386 0. 1189 0. 1081	200000 00000	7934 - 7923 - 7553 - 71353 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 71555 - 7	00000	40000 40000	6423 6423 6523 7573 1989	0.0017 0.0017 0.0018 0.0018	77 5 5 5 5 6 6 8 8	#####	66.66.65 66.66.62 66.66.62 66.66.62 66.66.63	0.0001 0.0004 0.0004 0.0003	16 7 8 N	00000	0.0047 -0.0004 -0.0007 -0.0006	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0000 0000 0000 0000 0000	2000
012 022 022 022		8 4 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	7. 861 7. 860 7. 860 7. 860 7. 860	78256	8 % % % % % % % % % % % % % % % % % % %		00000	0346 0217 0018 0235 0415	0.0895 0.0733 0.0510 0.0417 0.0473	00000	6365 5304 3407 0385	00000	20000 20000 20000 20000	. 2990 1. 2990 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	0.0000	020 04. 019 03. 016 01. 016 -00.	K M R M M	100 02 100 02 100 02 100 02	60606	00037 0037 00041 00047 00072	0016 0026 0028 0027	-0.0002 0.0007 0.0041 0.0040	11 11 11 11 11 11 11 11 11 11 11 11 11		00000	22227
024 027 030 030 030		0000000	0.000000000000000000000000000000000000	25 8 8 8 E		. 7007 . 7003 . 7711 . 7711 . 7511 . 7196		00000 M	0.1469 0.1263 0.1265 0.1166 0.1062		2000 7943 7634 7634 7264	00000 6	6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.532W 0.532W 0.532W 0.532W 0.532W 0.532W 0.532W	0.00017 0.00017 0.00017 0.00010	55588 S	\$ \$ \$ \$ \$ \$ \$	200000 200000 200000000000000000000000			0.0001 0.0001 0.0001 0.0001 0.001 0.001 0.001	0.00337			8000 8000 8000 8000 8000 8000	22229
} } }		<u> </u>		;			i		}																	

TABLE 2(B) (:LEAN HIRCRAFT A = 0°EIA(T) = -1 1/2°

	SIDE F	-0. 0027 -0. 0031 -0. 0070 -0. 0070	-0.0023 -0.0029 -0.0027 -0.0027	-0.003e	0.0000	0.0037 -0.0048 -0.0047 -0.0064	0.0046 -0.0046 -0.0046 -0.0037	-0.004 -0.00633 -0.00633 -0.00633 -0.00633
	RANG	11 11 11 11 11 11 11 11 11 11 11 11 11	4 4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6	44444 6666 00000	00000
	ROLL M	0.0008 0.0011 0.0009 0.0013 0.0001	0.0021 0.0030 0.0021 0.0003	0.0013 0.0001 0.0003 0.0012	0.0012 0.0034 0.0042 0.0031	0.0047 0.0064 0.0009 0.0043	0.0033 0.0034 0.0022 0.0023	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	VAK X	0.0020 0.0026 0.0028 0.0030 0.0031	0.0020 0.0020 0.0023 0.0023 0.0016	0.0025 0.0028 0.0028 0.0028	0.0025 0.0025 0.0026 0.0026	0.0025 0.0026 0.0027 0.0027	0.0027 0.0027 0.0027 0.0028	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	CR055.	0.0026 0.0046 0.0050 0.0069 0.0069	0. 0022 0. 0029 0. 0026 0. 0026	0.0037 0.0039 0.0052 0.0064	0.0015 0.0043 0.0043 0.0043	0.0044 0.0044 0.0064 0.0063	0.0044 0.0036 0.0039 0.0036	0.00044 0.000044 0.00000 0.00000
	St. 1P.	4 (00 00 00 00 00 00 00 00 00 00 00 00 00	20 .02 .(0.04 .(40 .02 -(30 .02 -(30 .02 -(30 .02 -(30 .02 -(30 .02 -(30 .02	95 - 100 . 04 44 - 100 . 04 90 - 100 . 04 40 - 100 . 04 38 - 100 . 04	31 - (00 .01 188 - (10 .02 95 - (10 .02 07 - (10 .01 40 - (10 .01	- (10 07 - 10	7 - (30 00 00 00 00 00 00 00 00 00 00 00 00 0
,×,	AT IC	18 03, 33 16 06, 25 15 -00, 94 13 -03, 45	2	18 03.34 14 -00.94 13 -03.09	8 6 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2000 C	16 06. 88 17 05. 88 17 05. 88 17 05. 37	2. 20. 25. 26. 20. 25. 26. 20. 26. 27. 26. 26. 27. 26. 26. 27. 27. 27. 27. 27. 27. 27. 27. 27. 27
41	. BASE.	31 0.005 14 0.005 22 0.005 63 0.005	0 0 001 0 0 001 0 0 001 0 0 001	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000	0.000	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
CLERW AJRCRAFT = 0 CELACIO = 0 CELACIO	. CL 50.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0,0023	0.633	0.0000	0.5296 0.5295 7.0.5360 9.0.4360	7 0 2457 7 0 0 0780 8 0 0 0780 8 0 0 0361 4 0 8 9 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8
E 39	- AXIAL	-0, 0360 -0, 0360 -0, 0360 -0, 0303 -0, 0303	-0.0310 -0.0310 -0.0278 -0.0275 -0.0253	-0.0273 -0.0353 -0.0373 2-0.0294 3-0.0294		.0.022 .0.034 .0.036 .0.028	0 -0.0196 -0.0160 -0.0547 -0.0539	-0.023 -0.033 -0.033 -0.023
	HORNAL	5 -0.3630 5 -0.3350 5 -0.0534 1 0.2329	-0.7967 -0.7705 -0.7499 -0.7499	-0, 5718 -0, 3070 -0, 0453 -0, 2442 -0, 8253	-0.8042 -0.7910 -0.7636 -0.7339	-0.5308 -0.2829 -0.0406 -0.2004	0. 7799 0. 7799 0. 7684 0. 7684 0. 6448	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	ORAG	0.0476 0.0476 0.0385 0.0441	0. 1284 0. 1184 0. 1066 0. 0998 0. 0789	0.0423	0, 1127 0, 1127 0, 1012 0, 0895 0, 0702	0. 0552 0. 0413 0. 0371 0. 1290	0, 1174 0, 1043 0, 0933 0, 0619	0.0528 0.0408 0.0361 0.0403 0.1198
	PITCH.	0.0395 0.0395 0.0395 0.0395	-0.0486 -0.0317 -0.0070 -0.0215	0.0292 0.0292 0.0443 0.0437	-0. 0345 -0. 0262 -0. 0125 0. 0029	0. 0306 0. 0306 0. 0392 0. 0504	0.0074 0.0074 0.0060 0.0162	0.0277 0.0312 0.0403 0.0533 -0.0203
	LIFT	0. 5597 0. 3339 0. 0539 -0. 2310	0.7868 0.7615 0.7427 0.7420	0. 3690 0. 3064 0. 0458 -0. 2423	0.7832 0.7832 0.7371 0.7396 0.6328	0. 5262 0. 2620 0. 0442 -0. 1987 0. 7699	0. 7935 0. 7730 0. 7457 0. 7649	0. 4989 0. 8687 0. 0378 -0. 1904 0. 7690 0. 7419
	3 MC 3 D	5 03. 33 6 01. 24 0 -(0. 94 0 -03. 11	1 06. 91 0 06. 41 1 05. 92 2 05. 42 9 04. 39	0 03.34 0 04.20 9 -00.94 0 -03.09	06.94 06.94 06.94 06.44 06.44 06.44 06.44	0 03, 34 0 01, 18 2 -00, 95 9 -03, 07	06.38 2 05.39 2 05.39 1 04.33	03. 25. 00. 95
	W. HRCH.	53 0.84 50 0.83 53 0.83 53 0.84	150 0. 801 150 0. 800 150 0. 801 150 0. 802	150 0. 600 150 0. 600 150 0. 799 150 0. 800 150 0. 751	55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	152 0. 750 152 0. 750 150 0. 752 152 0. 749 140 0. 700	440 0. 700 440 0. 701 439 0. 702 440 0. 700	137 0. 699 137 0. 699 140 0. 700 140 0. 502 140 0. 499
	SER REY	033 0.4 034 0.4 035 0.4	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4 4 0 4	200 200 200 200 200 200 200 200 200 200	057 0.4 058 0.4 050 0.4 050 0.4	055 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4 0. 650 0. 4	0000 0000 0000 0000 0000 0000 0000 0000 0000

TABLE 2(B) CLERN HJRCRAFT ETR = 0°ETR(T) = -1 1/2°

SIDE F	0.0024	0. 0043 0. 0055 0. 0066
RANG.	######################################	180. 0 -0. 0 180. 0 -0. 0 180. 0 -0. 0
MOLL N	0.0017 0.0017 0.0020 0.0023	0. 0013 0. 0013 0. 0015
YAK K	0.0027 0.0027 0.0027 0.0027 0.0026	0.0022 0.0025 0.0025
CROSS.	0.0023 0.0029 0.0030 0.0040	0. 0042 0. 0054 0. 0065
SUIP	(0.04 (0.04	- 100.02 - 100.02 - 100.02
AZ MC.	95. 25 93. 25 93. 25 93. 25 93. 25	04. 10 -00. 97 -03. 04
BASE.	0.0018 0.0020 0.0020 0.0018 0.0018	0. 0017 0. 0014 0. 0014
ניר צם	0, 4994 0, 4415 0, 3825 0, 2774 0, 1854	0. 0549 0. 0009 0. 0293
AX 1AL.	10.0101 10.0099 10.0108 10.0157	-0.0323 -0.0343 -0.0282
RORMAL	-0.6692 -0.6692 -0.6224 -0.5294	-0. 2353 -0. 030 6 0. 1734
DRAG	0.0896 0.0787 0.05696 0.0563	0. 03 65 0. 0351 0. 0307
P1TCH.	0070 0438 0476 0212 0239	0313
JHGJD. LIFT.	06.27 0.7065 0. 105.76 0.6646 0. 105.24 0.6185 0. 104.21 0.5266 0. 03.17 0.4307 0.	0. 2345 0. 0313 -0. 1717
1 NC 1 D.	06. 27 05. 76 05. 24 04. 21 03. 17	01. 10 -00. 97 -03. 04
SER REYN, MACH.	077 0.440 0.500 078 0.440 0.500 079 0.440 0.500 080 0.440 0.501	c. 499 c. 500 c. 499
REYK.	00000	0.440
); F1	077 078 079 080 081	0 0 0 0 0 0 0

TABLE 2(C) CLERN AJRCRAFT ETA = 0°ETA(T) = 3/2

7	0017 0018 0018 00018	0000 0000 0000 0000 0003 0003	0000 0000 00018 00018 00018	00018 00008 0008 00043	0018 0018 0017 0017	0000	0018 0007 0008 0008 0018	9000 8000 9000 9000 9000
810			00000		00000		88888 66666	0000 9899
Ę					00000	00000	00000	0000
RANG		7777	14444 1444 1444 1444 1444 1444 1444 14	44444	44444 600000000000000000000000000000000		12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
-i ≖	0000	00004 0010 0014 0018 0022	0010 0013 00016 0007 0005	0001 0010 0013 0018 0018	0003	00013 0013 0017 0016 0021	0000 0000 0000 0000 0000	0003 0013 0017 0016
ROLL	9 9 9 9	00000	00000	00000	00000	00000	00000	0000
zi -	00010 00013 00013 00014	0000 0000 0000 0000 0000	0010 0013 0013 0015 0012	0000 0000 0000 0000 0000 0000	00011 00011 00014 00014	00000 00000 00000 00000	00011 00012 00012 00014	0001 00003 00002
¥ >	00000	0000	0000	00000	9999	00000	99999	0000
CROSS.	00016 00016 00018 00016	00001 0000 0 00007 0030	00016 00019 0013 0013	00013 00002 00008 00022 00042	0013 0013 0021 0014 0011	0000 0000 0000 0000 0000	0004 0000 0004 0022 0013	0007 0003 0015 0010
<u> </u>	6000	00000		00000	99999	00000	0000	9999
<u>.</u>	88888	88888	88888	8888	88888	8888	88888	90.00
뷺	55855	~ * * * * * * * * * * * * * * * * * * *	88888	88888	55555	23886	55555	8888
ATNC.	07. 43 06. 34 05. 38 05. 33	04. 35 03. 26 03. 14	05. 43 06. 39 05. 43 05. 43	04. 32 03. 23 03. 13	05. 40 05. 40 05. 40	04. 44 00. 40 00. 40 03. 63 03. 63	06. 30 06. 30 05. 40 05. 38	96. 20 96. 20
		6 1		00000	020	40.60		0200
BASE.	0.0023 0.0023 0.0024 0.0024	0.0022 0.0024 0.0024 0.0049	0.0024 0.0024 0.0024 0.0024	0.0000		0.0000	0.0001	
		0.00.00.00		48048				0. ED M M
נורצם	0, 765 0, 703 0, 636 0, 572 0, 572 0, 549	0. 2964	0, 7036 0, 6791 0, 6246 0, 5677 0, 5077	00000	0. 6686 0. 6388 0. 6291 0. 5767 0. 5181	0, 4159 0, 3139 0, 1220 0, 0040 0, 0578	0. 6658 0. 6228 0. 5077 0. 5918 0. 5336	0. 434
		94484 F4748	8 4 8 W 4	2222	79 4 6 6 7 9 6 6 6	*****		
RXIAL	0. 0556 0. 0528 0. 0509 0. 0500	00000 00000	20022	22225	00000	88888	0. 03 87 0. 0376 0. 0344 0. 0363	0. 0336 0. 0349 0. 0380 0. 0383
	: : : :	20 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 1 1 1 1	9 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1 1 1 1 1		1 : : : :	: : : :
PORM	0. 8516 0. 8516 0. 7661 0. 7561		0.8362 0.8362 0.8008 0.7623 0.7202		0. 8306 0. 8230 0. 8033 0. 7678 0. 7267	0. 5500 0. 3538 0. 3505 0. 0639 0. 2428	0. 7999 0. 7999 0. 7999 0. 7774 0. 7374	0, 6615 0, 3768 0, 3466 0, 0577
	727 - (574 - (489 - (207 - (24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1937 - (1938 - 1	0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1887 - 1700 - 17
DRAG	00000	0.0000	00000	0.0.0.0 0.0.0.0	0.0.0.0.0	0.000	0.0.0.0.0 444440	0000
z i			M	64400		AL		1274
PITCH	0.120	0. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0. 091 0. 092 0. 097 0. 098	0.0000	0.1027 0.0967 0.0875 0.0785 0.0704	0.033	0. 1032 0. 0786 0. 0721 0. 0699 0. 0591	0000
_	11111	**************************************		1 1 1 1		1 1 1	11111	1 7 7
LIFT	0. 875 0. 797 0. 797 0. 725 0. 725	0.0.0.0.0	0.8241 0.7904 0.7535 0.7535	0. 5342 0. 3479 0. 3393 0. 0671 0. 2571	20000	0.0604 0.0604 0.0604 0.0648	0. 8160 0. 7892 0. 7796 0. 7693 0. 7305	0. 6567 0. 5736 0. 3456 0. 0583
	4 % W O W W 4 % V R	4 6 4 9 4 4 6 4 9 4	A S W P W	22 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5 4 5 8 V	*	8008 X	8 2 2 3 8 2 2 3
18010	28.588	2888	28889	2888	2 8 8 8	22232	28888	25.25
Ž	807 807 807 806 806	900 900 900 900 900 900	880 880 878 878	879 873 873 879	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	#559 #61 1660 1650	2	841 833 841 840
KACH	ರವರದ ಕಾರ್ಚಕ	ತರಕರದ	ತರಕರ	ರದರೆದೆ	4000	ರದ ಪರಕ	ೆಕೆಕೆಕ	6566
RE VR.		0. 435 0. 435 0. 439 0. 439	0.00 0.432 0.432 0.422 0.423	0.432 0.432 0.432 0.432	44444	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0. 437 0. 437 0. 437 0. 437	0.000
SER	0.990 0.991 0.993 0.995 0.996 0.996	097 098 099 100 101	2010 1010 1010 1010 1010 1010	107 108 1109 1110	111111111111111111111111111111111111111	1113 1113 1113 1113 1113 1113 1113 111	2000	2242
•1			राक्षाचाकाची	र अस्त स्त्री	************	राच्या समि		નન નન

TABLE 2(C) CLERN HIRCRAFT ETR = 0 ETR(I) = -1/2

M. ROLL M RANG. S	103 0.0019 180.0 - 107 0.0026 180.0 - 107 0.0021 180.0 - 107 0.0023 180.0
IP. CROSS. YAN	10. 01 0. 0025 0. 0007 10. 00 0. 0000 -0. 0007 10. 00 0. 0000 -0. 0007 10. 00 -0. 0005 -0. 0008
BASE. ATHC. SL	0.0043 -03.42 -00 0.0020 07.42 00 0.0048 06.94 00 0.0048 06.44 00 0.0049 05.93 00
AXIAL. CLSO.	0, 0300 0, 0337 0, 0333 0, 6568 0, 0340 0, 6477 0, 0298 0, 5487 0, 0298 0, 5447
DRAG KORHAL A	1412 -0.820 -1.306 -0.849 -1.200 -0.7953 -1.206 -0.7628 -1.206 -0.7628 -1.206 -0.7628 -1.2064 -0.7628 -0.7628 -1.2064 -0.7628
. PITCH. D	322 0.0264 0.105 -0.0717 0.069 -0.0787 0.0867 -0.0620 0.0543 0.0544 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.0554 0.05
INCID. LIFT.	03. 12. 0. 2 06. 94. 0. 8 06. 41. 0. 7 07. 93. 0. 7
MRCH.	37 0. 840 55 0. 802 55 0. 800 55 0. 801 55 0. 801

TABLE 2(C) CLEAU RINCRAFT ETA = 0 ETA(T) = -1/2

L.	348
SIDE F	180, 0 -0, 0016 180, 0 -0, 0021 180, 0 -0, 0022
RANG	180.0 180.0
ROLL M	0.0019 0.0021 0.0022
YAK N.	0.0001 0.0001 0.0001
CROSS.	0, 0015 0, 0020 0, 0027
StiP	(10° 00 (10° 00 (10° 00
ATHC.	04, 40 -00, 98 -03, 05
BASE.	0, 0016 0, 0014 0, 0013
נר 20.	0, 0589 0, 0012 0, 0275
AX I AL.	2437 -0.0309 0358 -0.0332 1681 -0.0271
RORMAL	-0.2437
DRAG	0, 0371 0, 0340 0, 0372
PITCH.	0. 0146 0. 0256 0. 0392
LIFT.	0. 2429 0. 0363 -0. 1664
JHCJD. LIFT.	04. 10 -00. 98 -03. 05
нясн.	a. 500 a. 499 p. 504
SER REVN	175 0, 431 0, 500 01, 10 0, 2429 176 0, 431 0, 499 -00, 98 0, 0363 177 0, 431 0, 501 -03, 05 -0, 1664

TABLE 2(D) CLERN HJRCRAFT ETA = 0 ETR(T) = +1/2°

SIDE F	0.0033 0.0033 0.0030 0.0030	0.0033 0.0013 0.0013 0.0013	0.0063 0.0046 0.0046 0.0036	0.000 00 00 00 00 00 00 00 00 00 00 00 0	0.003 0.003 0.003 0.003	000000000000000000000000000000000000000	
RANG.	4 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	4 4 4 4 4 4 4 6 6 0 0 0 0 0 0 0 0 0 0 0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	180.0 180.0 179.9	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
ROLL M	0.0001 0.0006 0.0012 0.0007	0.0007 0.0011 0.0014 0.0016 0.0015	0. 0004 0. 0000 0. 0007 0. 0008	0,0002 0,0012 0,0013 0,0016 0,0014	0.0044 0.0046 0.0004 0.0004	0.0003 0.0012 0.0016 0.0014 0.0014	0.00044 0.000442 0.000442 0.00001 0.0002
YAN H.	-0.0006 -0.0013 - -0.0009 - -0.0012 -	0, 00010 0, 00007 0, 00005 0, 00000	0.0015 0.0012 0.0012 0.0012	0. 0012 0. 0008 0. 0003 0. 0001	0.0008 0.0009 0.0012 0.0011	0.0003 0.0003 0.0003 0.0004	0.0000 0.0000 0.0000 0.00011 0.0012
CROSS.	0.0036 0.0054 0.0031 0.0040	0.0036 0.0029 0.0008 0.0009	0,0064 -0,0049 -0,0042 -0,0039 -0,0039	0.0032 0.0000 0.0000 0.0000	-0.0033 -0.0059 -0.0054 -0.0050	0, 0033 0, 0003 0, 0000 0, 0000	0.0026 0.0026 0.0026 0.0033 0.0033 0.0033 0.0033 0.0033
St. 1P.	30.00 30.00 30.00 30.00 30.00	20.00 20.00 20.00 20.00 20.00 20.00 20.00	20.00 20.00 20.00 20.00 20.00 20.00	(10, 00 (10, 00 (10, 00 (10, 01 (10, 01 (10, 01	(10.00 (10.00 (10.00 (10.00 (10.00 (10.00	(0.00 - (0.00	6.000 6.000
A 1 IC.	07.00 06.92 05.93 05.94 05.94	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	07. 44 06. 94 05. 88 05. 86	04. 27 00. 27 00. 27 00. 29	00000000000000000000000000000000000000	04. 23 00. 23 04. 23 00. 43 04. 44	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
RASE.	0. 0024 0. 0024 0. 0023 0. 0022 0. 0022	0.0024 0.0024 0.0020 0.0024 0.0024	0.0013 0.0024 0.0024 0.0023 0.0024	0.0024 0.0049 0.0049 0.0049	0.0016 0.0018 0.0021 0.0021	0. 0019 0. 0018 0. 0018 0. 0018 0. 0019	0.0019 0.0019 0.0019 0.0018 0.0024
CL SQ.	0, 7208 0, 6703 0, 6099 0, 5643 0, 5643	0, 4068 0, 2945 0, 1003 0, 0024 0, 0024	0, 6994 0, 6655 0, 6142 0, 5620 0, 5620	0, 4063 0, 3012 0, 1160 0, 0053 0, 0053	0, 6359 0, 6303 0, 6267 0, 5769 0, 5167	0, 4161 0, 3169 0, 1246 0, 0055 0, 0522	0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
RX J.R.L.	-0, 0543 -0, 0541 -0, 0508 -0, 0504 -0, 0504	-0.0508 -0.0503 -0.0520 -0.0474 -0.0474	-0.0483 -0.0463 -0.0482 -0.0444 -0.0444	-0, 0432 -0, 0449 -0, 0463 -0, 0430	-0. 0439 -0. 0389 -0. 0340 -0. 0395	-0. 0394 -0. 0390 -0. 0424 -0. 0377	0.0342 0.0342 0.0344 0.0344 0.0344
RORNAL	-0. 8637 -0. 8317 -0. 7919 -0. 7607	-0, 6438 -0, 5468 -0, 3484 -0, 0487 0, 2508	-0, 8502 -0, 8278 -0, 7944 -0, 7586	-0, 6428 -0, 5522 -0, 3420 -0, 0728	-0. 8229 -0. 8050 -0. 8016 -0. 7679 -0. 7273	-0.5565 -0.35655 -0.35655 -0.0744	0.000000000000000000000000000000000000
DRAG	0, 1676 0, 1562 0, 1406 0, 1298 0, 1196	0, 1011 0, 0832 0, 0601 0, 0487 0, 0584	0, 1599 0, 1476 0, 1333 0, 1240 0, 1119	0.0933 0.0583 0.0534 0.0436	0.1519 0.1379 0.1321 0.1194	0, 0902 0, 0733 0, 0513 0, 0383	0 0 1136 0 0 1136 0 0 1136 0 0 0 1166 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
P1TCH.	-0. 0939 -0. 0970 -0. 1034 -0. 1074 -0. 1076	-0. 1039 -0. 0924 -0. 0717 -0. 0369 0. 0106	-0.0812 -0.0989 -0.1002 -0.1007 -0.0966	-0.0833 -0.0737 -0.0849 -0.0869	-0. 0634 -0. 0387 -0. 0977 -0. 0925	-0. 0707 -0. 0334 -0. 0343 -0. 0143	-0.00 th 0.00
LIFT.	0.8491 0.8188 0.7810 0.7513 0.7154	0. 6379 0. 3429 0. 3469 0. 0495	0.8364 0.8359 0.7838 0.7838 0.7497	0. 5430 0. 3490 0. 0430 0. 0735	0. 8099 0. 7940 0. 7917 0. 7596 0. 7203	0. 6452 0. 5631 0. 3533 0. 0748	0. 844 0. 7947 0. 7907 0. 7687 0. 7348 0. 6398
JHCJD.	07. 43 06. 92 06. 38 05. 86 05. 34	04. 29 03. 24 04. 42 04. 04 03. 15	07. 44 06. 91 06. 39 05. 86 05. 34	04.34 03.27 04.45 -00.99	07. 44 06. 95 06. 39 05. 38 05. 88	04, 33 03, 29 04, 46 -00, 97	0.5 % % % % % % % % % % % % % % % % % % %
касн.	C. 303	2. 300 2. 300 2. 300 2. 300 300 300 300	6 0. 884 6 0. 884 7 0. 884 7 0. 880 10. 879	0.879 0.880 0.881 0.881 0.881	C. #60 C. #60 C. #60	0.860 0.861 0.861 0.861	0.0 844 0.0 844 0.0 844 0.0 842 0.0 843
SER REYN.	002 0, 458 003 0, 458 004 0, 457 005 0, 457	007 0.457 008 0.457 009 0.457 010 0.457	014 0.455 015 0.457 016 0.455 017 0.457 018 0.457	019 0, 458 020 0, 458 021 0, 458 022 0, 458 023 0, 458	026 0.457 027 0.457 028 0.457 029 0.457 030 0.457	031 0, 457 032 0, 455 033 0, 457 034 0, 457 035 0, 458	038 0.463 040 0.467 041 0.463 042 0.463 042 0.463
⊕ :							88666

TABLE 2(D) CLEAN AJRCRAFT ETA = 0° ETA(T) = +1/2°

SIDE F	0.0021 0.0003 0.0007 0.0020 0.0037	0.0034 0.0021 0.0027 0.0039 0.0042	0, 0025 0, 0016 -0, 0003 -0, 0014	0. 0030 0. 0017 0. 0003 0. 0003	0.0027 0.0013 0.0013 0.0003	0,0025 0,0015 0,0016 0,0016	0.0022 0.0041 0.0041 0.0001 0.0007
RANG.	180.0 180.0 180.0 180.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 1 80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	180.0 180.0 180.0 180.0	11 11 11 11 11 11 11 11 11 11 11 11 11	11 11 11 11 11 11 11 11 11 11 11 11 11
ROLL M	0.0015 0.0019 0.0015 0.0020 0.0020	0.0029 0.0039 0.0028 0.0007 0.0007	0.0021 0.0016 0.0014 0.0014 0.0016	0.0028 0.0039 0.0049 0.0033	0.0019 0.0021 0.0016 0.0015 0.0017	0.0038 0.0040 0.0038 0.0038	0.0028 0.0028 0.0015 0.0015 0.0015
Y X	-0.0008 0.0001 0.0000 0.0000 0.0002 -0.0012	-0.0009 -0.0005 -0.0004 -0.0009	-0.0003 -0.0004 -0.0004 -0.0002	-0.0004 0.0002 0.0003 0.0004	-0, 0004 -0, 0002 -0, 0004 0, 0000	0. 00001 0. 00003 0. 00003 0. 00003	0.00001
CROSS.	-0.0022 0.0006 0.0006 0.0019	-0,0033 -0,0022 -0,0028 -0,0040	-0.0026 -0.0017 0.0002 0.0013	-0, 0031 -0, 0018 -0, 0004 -0, 0004	-0.0028 -0.0016 -0.0014 0.0004	-0.0026 -0.0016 -0.0013 -0.0017	-0.0023 -0.0012 -0.0002 0.0002 -0.0002
St. 1P.	(10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,00 (10,000 (10,00 (10,00) (10,00	(10, 00, 00, 00, 00, 00, 00, 00, 00, 00,	(10.01 (10.01 (10.00	00000000000000000000000000000000000000	(10, 01 (10, 01 (10, 01 (10, 01 (10, 01	.00.01 .00.01 .00.01 .00.01	-000.01 -000.01 -000.01 -000.01 -000.01
A I HC.	03. 34 04. 49 -00. 97 -03. 44	06, 89 06, 38 05, 88 05, 88	03, 32 01, 18 -00, 97 -03, 11	06. 89 06. 39 05. 89 04. 44	04. 36 03. 29 04. 16 -00. 97 -03. 10	07. 38 06. 86 06. 37 05. 86	04.34 03.25 04.44 -00.97 -03.08
BASE.	0, 0017 0, 0013 0, 0017 0, 0015 0, 0015	0,0018 0,0017 0,0017 0,0018 0,0018		0.0017 0.0016 0.0017 0.0013	0, 0018 0, 0013 0, 0017 0, 0016 0, 0016	0.0017 0.0017 0.0017 0.0017 0.0017	0, 0017 0, 0016 0, 0016 0, 0017 0, 0013
CLSQ.	0, 3346 0, 1246 0, 0045 0, 0476 0, 6853	0, 6408 0, 6244 0, 6045 0, 5720 0, 4690	338 103 003 039	0, 6419 0, 5591 0, 5959 0, 5329 0, 4303	0, 4503 0, 2963 0, 0886 0, 0030	0, 6459 0, 6530 0, 6734 0, 5734 0, 5734	0, 3929 0, 2609 0, 0027 0, 0310 0, 6113
HXIAL.	-0. 0354 -0. 0403 -0. 0378 -0. 0342	-0.0311 -0.0296 -0.0267 -0.0267	₩ ₩₩₩	-0.0224 -0.0224 -0.0480 -0.0480	-0.0182 -0.0223 -0.0339 -0.0350	-0. 0235 -0. 0235 -0. 0453 -0. 0433	-0.0551 -0.0221 -0.0326 -0.0326 -0.0283
HORMAL	0. 5792 0. 3500 0. 0675 0. 2206 0. 3395	0.8404 0.7967 0.7847 0.7625 0.6891	0, 3842 0, 3230 0, 0606 0, 1998 0, 8379	0, 8103 0, 8009 0, 7784 0, 7353 0, 6747	0, 6747 0, 3468 0, 2988 0, 0551 0, 1854	-0, 81.65 -0, 79.63 -0, 76.63 -0, 75.53	-0.5301 -0.5132 -0.2843 -0.0515 0.1782
DRAG	0, 0704 - 0, 0494 - 0, 0384 - 0, 0447 - 0, 1428 -	0, 1298 0, 1197 0, 1086 0, 1000	0617 0427 0366 1336	0, 1228 - 0, 1127 - 0, 1012 - 0, 0892 - 0, 0713 -	0, 0543 - 0, 0536 - 0, 0445 - 0, 0356 - 0, 0399	0, 1295 0, 1171 0, 1052 0, 0931	0.0641 0.0328 0.0358 0.0353 0.1481
P11CH.	-0.0425 -0.0235 -0.0060 -0.0037	-0. 0841 -0. 0825 -0. 0789 -0. 0537	016 007 000 000 008	-0.0534 -0.0587 -0.0466 0.0088	-0. 0074 -0. 0046 -0. 0040 0. 0143	-0. 0351 -0. 0357 -0. 0402 -0. 0274 -0. 0174	-0.0068 -0.0087 -0.0088 0.0089 -0.0176
LIFT.	0. 5760 - 0. 3489 - 0. 0681 - 0. 2186 0. 8279 -	8 4 4 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	3815 3221 0611 1980	M & D D &	0. 6712 0. 5444 0. 2979 0. 0556 0. 1837	0.8082 0.8082 0.7894 0.7598	0.6269 0.5110 0.2834 0.0320 -0.1764
) RC 1 D.	03, 34 04, 49 -00, 97 -03, 44 07, 39				04. 36 03. 29 01. 16 00. 97	07. 38 06. 86 06. 37 05. 86	04. 34 03. 25 04. 44 -00. 97 -03. 08
KACH.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ರಕ್ಕೆ ಕ	: ವರದರದ		0. 751 0. 750 0. 749 0. 749 0. 749	C 702 C 704 C 704 C 700 C 704	ರಕಕಕರ ಕ
ER REVN.	48686	- ಕಟ್ಟೆಟ್ಟೆ - ಕಟ್ಟೆಟ್ಟೆ - ಈ ಚಿಕ್ಕಳ			062 0.457 069 0.457 070 0.457 071 0.457 072 0.457	075 (1, 442) (176 (1, 442) 077 (1, 442) 078 (0, 442)	- 55555 5 - 74444 4
ಪ	5 5 5 5 5	5555	. 55555		90000	66 66 66	55555

TABLE 2(D) CLEGH R)RCRRFT ETA = 0° ETR(T) = +1/2°

2. R	REVIE.	SER REVN. ISCH.	JRCJD.	LIFT.	PITCH.	DRAG	HORMAL	AXIAL.	CL SQ.	BASE.	ATRC.	St. 19.	CROSS.	* AE *	ROLL M	RANG.	SIDE
0.880 0.890 0.890 0.890	4 4 4 4 4 4 4 2 0 0 0 0 0 0 0 0 0 0 0 0	0. 440 0. 501 0. 440 0. 501 0. 440 0. 501 0. 440 0. 501 0. 437 0. 499	06. 26 06. 25 05. 25 05. 25	0, 7584 0, 7584 0, 7212 0, 6802 0, 6304	-0.0352 -0.0352 -0.0249 -0.0182	0. 1035 0. 1035 0. 0903 0. 0796	-0.7634 -0.7634 -0.7268 -0.6849	7554 -0.0415 7654 -0.0415 7268 -0.0094 6849 -0.0092	0, 5754 0, 5754 0, 5200 0, 4626 0, 3973	0.0018 0.0018 0.0018 0.0019 0.0017	06.27 06.28 05.28 05.28	(10, 01, 01, 01, 01, 01, 01, 01, 01, 01,	-0.0027 -0.0027 -0.0032 -0.0030	0.0006 0.0006 0.0005 0.0005	0.0024 0.0024 0.0022 0.0024 0.0024	180.0 0.008 180.0 0.008 180.0 0.008 180.0 0.008	0.0000
299 299 299 299 799	0.0.0 4.4.4.0.0 2.4.4.4.0.0 2.4.4.4.0.0	093 0, 440 0, 499 094 0, 440 0, 501 095 0, 440 0, 501 096 0, 440 0, 499	04, 19 03, 16 04, 09 00, 98 03, 05	0, 5392 0, 4455 0, 2499 0, 0464 0, 1575	-0.0105 -0.0078 -0.0005 0.0095	0.0564 0.0473 0.0375 0.0339	0. 5475 0. 2567 0. 0459 0. 1592		0, 2906 0, 1983 0, 0624 0, 0220 0, 0247	0, 0048 0, 0047 0, 0047 0, 0045 0, 0045	04, 19 - (00, 01 - 03, 16 - (10, 01 - 00, 09 - (10, 01 - 00), 98 - (10, 01 - 03, 05 - (10, 01 - 03, 05 - (10, 01	(10, 01, 01, 01, 01, 01, 01, 01, 01, 01,	0, 0017 0, 0012 0, 0003 0, 0003	0.0005 0.0004 0.0002 0.0001	0.0026 0.0024 0.0018 0.0016 0.0016	180. 0 0.001 180. 0 0.001 180. 0 0.000 180. 0 -0.000	0. 000 0. 000 0. 000 0. 000 0. 000

TABLE 2(E) CLERIE H)RCRRET ETR = 0° ETR(T) = +1 1/2°

SIDE F	0.0010 0.0000 0.0001 0.0022 0.0052	0.0006 0.0011 0.0038 0.0052 0.0052	0. 0018 0. 0007 0. 0006 0. 0011	0. 0009 0. 0026 0. 0035 0. 0047 0. 0073	0.0001 0.0008 0.0002 0.0002	0.0006 0.0020 0.0031 0.0042	0.0001 0.0001 0.0001 0.0013 0.0013
R 8 6	474 99,99,99 47,99,99	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	180.0 179.9 179.9 179.9	179.9 180.0 180.0 180.0	180.0 179.9 179.9	179.9 180.0 180.0 180.0	14 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
ROLL M	-0.0004 -0.0008 -0.0019 -0.0012	0. 0001 0. 0006 0. 0009 0. 0012 0. 0014	0, 0012 -0, 0003 -0, 0011 -0, 0012 -0, 0006	-0.0002 0.0008 0.0010 0.0013 0.0011	0.0045 0.0007 -0.0008 -0.0008	-0.0001 0.0008 0.0011 0.0010	0.0037 0.0028 0.0028 0.0007 -0.0007
Y M	0.0011 0.0012 0.0011 0.0011	0.0014 0.0006 0.0022 0.0023	0.0013 0.0011 0.0012 0.0013 0.0011	0. 0015 0. 0021 0. 0028 0. 0024 0. 0024	0.0000 0.0013 0.0012 0.0011	0,0013 0,0017 0,0024 0,0024 0,0024	0. 0012 0. 0012 0. 0012 0. 0012 0. 0011
CR055.	-0.0010 -0.0001 -0.0002 0.0021 0.0021	0, 0005 0, 0010 0, 0037 0, 0051 0, 0065	-0.0019 -0.0008 0.0003 0.0010	0.0008 0.0025 0.0034 0.0046	-0.0002 -0.0003 -0.0003 -0.0003	0.0003 0.0019 0.0030 0.0041	0.00000
SLIP	- (10, 01 - (10, 01 - (10, 01 - (10, 01 - (10, 01 - (10, 01	100.01 100.01 100.01 100.01	(0) 01 (0) 01 (0) 01 (0) 01	100.02 100.02 100.02 100.02	(00.01 (00.01 (00.01 (00.01	.00.01 -00.01 -00.02 -00.02	20000000000000000000000000000000000000
RJIC.	07, 42 06, 90 06, 37 05, 84 05, 32	03. 22 03. 22 04. 44 03. 03	06. 90 06. 90 06. 88 05. 88	04.29 03.28 04.14 -01.00	07, 40 06, 93 06, 38 05, 86	04.34 03.27 04.46 -00.99	00.00 00
: +1 1/2 BASE.	0, 0022 0, 0022 0, 0024 0, 0024 0, 0024	0.0022 0.0022 0.0022 0.0022 0.0022	0, 0024 0, 0023 0, 0023 0, 0024 0, 0024	0.0024 0.0028 0.0018 0.0019	0,0023 0,0022 0,0020 0,0022 0,0023	0, 0024 0, 0024 0, 0049 0, 0049 0, 0044	0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.
ETACT) = CLSQ.	0, 7274 0, 6737 0, 6485 0, 5667 0, 5187	0, 4171 0, 3061 0, 1087 0, 1036 0, 1036	0, 6850 0, 6707 0, 6183 0, 5672 0, 5586	0, 4172 0, 3132 0, 1230 0, 0069 0, 0545	0, 6374 0, 6374 0, 6359 0, 5359 0, 5335	0, 4292 0, 3236 0, 1319 0, 0067 0, 0500	0.5636 0.6274 0.6274 0.6274 0.6274 0.6274 0.6274
ETR = 6° RXIRL.	-0, 0360 -0, 0533 -0, 0520 -0, 0504 -0, 0499	-0.0500 -0.0511 -0.0516 -0.0474 -0.0474	.0.0455 .0.0455 .0.0448 .0.0448	-0.0452 -0.0453 -0.0462 -0.0443	-0. 0446 -0. 0382 -0. 0445 -0. 0397 -0. 0383	-0, 0392 -0, 0403 -0, 0422 -0, 0399	-0.0417 -0.0393 -0.0393 -0.0364 -0.0360
HORMAL	-0.8679 -0.8337 -0.7976 -0.7623	-0.6517 -0.5574 -0.3312 -0.0597 0.242	-0, 8411 -0, 8310 -0, 7967 -0, 7620 -0, 7277	-0 6515 -0 2635 -0 8921 -0 8821 -0 2861	-0. 8235 -0. 8233 -0. 6235 -0. 7347	-0,6603 -0,5725 -0,3644 -0,0817 0,2261	0.7828 -0.7828 -0.7828 -0.7857 -0.7857
DRAG	0, 1699 0, 1552 0, 1426 0, 1303 0, 1196	0. 1006 0. 0845 0. 0601 0. 0484 0. 0570	0, 4562 0, 4482 0, 4353 0, 4240 0, 435	0.0938 0.0793 0.0549 0.0438 0.0438	0, 1528 0, 1378 0, 1330 0, 1207 0, 1091	0.0908 0.0749 0.0514 0.0402 0.0463	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
P1TCH.	-0.1083 -0.1144 -0.1200 -0.1222 -0.1265	-0. 1262 -0. 1169 -0. 0960 -0. 0586 -0. 0071	-0.0706 -0.1095 -0.1128 -0.1167	-0.1084 -0.0986 -0.0784 -0.0503	-0.1014 -0.0596 -0.1087 -0.1141 -0.1100	-0.0936 -0.0838 -0.0619 -0.0368	-0.11155 -0.0766 -0.0766 -0.0618 -0.1038
LIFT	0, 8529 0, 8209 0, 7865 0, 7528 0, 7503	0.6459 0.5534 0.3300 0.0604 -0.2415	0. 8277 0. 8191 0. 7864 0. 7531 0. 7502	0. 6460 0. 3598 0. 3510 0. 0834 0. 2338	0. 8125 0. 7984 0. 7975 0. 7663 0. 7304	0.6552 0.5691 0.3633 0.0823	0.000 0.700 0.700 0.700 0.777 0.777 0.777
J RCJ D.	07.42 06.90 06.90 05.84 05.84	04. 27 03. 22 04. 44 04. 03	06, 30 06, 30 06, 38 05, 88 05, 88	04. 25 03. 25 04. 44 -04. 00	07. 40 06. 93 06. 38 05. 86 05. 86	04. 34 03. 27 08. 46 -00. 99	00.000 006.934 006.934 005.424
RACH	5 0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	5 (c. 899 5 (c. 899 7 (c. 900 7 (c. 900 7 (c. 900	7 (1.879 7 (1.879 5 (1.880 8 (1.881 8 (1.881	C. REC R. C. REC R. C. REC R. C. R. 29 R. C. REC R. C. REC R. R. 29	0 0.861 0 0.861 0 0.861 0 0.861	7 C. 863 7 C. 863 7 C. 860 8 C. 850 6 C. 851	
R REVK.	20000 44444 88888	00000 44444 80000	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000	6 0, 460 8 0, 460 9 0, 460 9 0, 460	2 0.460 2 0.460 3 0.437 0.438	24444 £
Ü	000 000 000 000 000 000 000	000 000 010 011	0 0 0 0	020 020 021 022 022	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22222

TABLE 2(E) CLEAN HINCRAFT ETA = 0° ETH(T) = +1 1/2°

I A.	00000 00019 00019 00019	00110	0000 0000 0000 0000	2 1 2 1 2	2 4 8 4 5 2 4 8 4 7		
SIDE	00000	0.0009 0.0020 0.0011 0.0014	00000	0.001; 0.001; 0.002; 0.002;	0.0019 0.0032 0.0038 0.0047 0.0057	0.0022 0.0032 0.0039 0.0029	0.00000 0.00000 0.00000 0.00000 0.00000
ø	00000	00000	00000	00000	00000	00000	00000
7	1 1 8 0 0 1 1 8 0 0 0 1 1 8 0 0 0 1 1 8 0 0 0 1 1 8 0 0 0 1 1 8 0 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 8 0 0 1 1 1 1	4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 8 0 0 1 1 8 8 0 0 1 1 8 8 0 0 1 1 8 8 0 0 1 1 8 8 0 0 1 1 8 8 0 0 1 1 1 1	1 1 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
E	2000	00009 0029 0020 0020	0007 0016 0011 0009	0016 0018 0034 0033	0016 0018 0012 0014	0036 0038 0039 0028	0023 0010 0010 0013 0024
ROLL			00000	88888			
ž	0015 0015 0025 0024	0011 0015 0015 0014	0018 0021 0023 0023	00020 00020 0020 0020	00022 00024 00024 00023	0053 0023 0023 0023 0023	0022 0024 0024 0024 0024
ž Š		88888	00000	00000	00000		
Ş	00000 00010 00031	00019 0019 0013 0013	0017 0029 0039 0043	0111 024 032	0018 0031 0037 0046	0021 0021 0029 0028	0032 0027 0047 0052 0053
CRO	66666	66666	88888	99999	66666	00000	
۵	1000 1000 1000 1000 1000 1000 1000 100	55555	22222	55555	55555	55555	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
175			55555		55555	5555	
1.8C.	W W W W W W	M	E C 6 6 4	# # # # C	W W M W M	W B W B W	W W H W W W W W W W W W W W W W W W W W
ē	90000 4 4 0 6	00000	40000	00000	20200	00000	4000
SE.	0022 0024 0020 0019 0017	0013 0022 0020 0021 0021	0022 0018 0018 0018	0020 0020 0020 0020 0020	0019 0020 0016 0017 0017	0018 0020 0018 0024 0024	0020 0013 0013 0015 0015
	80000	00000	00000	00000	56556	စ်စ်စ်စ်စ်	00000
180	4465 3427 1286 0007 0431	6936 6580 6270 6155 5875	4840 3481 0483 0483	6989 6679 6411 5410	4594 3056 0942 0043 0308	6794 6734 6739 5347	4048 2730 0856 0038 0277 6284
נרצ	00000	00000	00000	00000	66666	56666	00000
7 E	0336 0344 0386 0386 0389	0349 0347 0308 0278 0252	0250 0267 0345 0359	0272 0245 0225 0136	0179 0230 0342 0365 0265	0245 0497 0457 0440 0440	0162 0325 0325 0325 0325 0232
¥ X	55575		2 4 5 5 5	\$ \$ \$ \$ \$ \$	င့် ဝှ ဝှ ဝှ ဝှ	6 6 6 6	
RAR	6730 5886 3598 0758	8447 8213 8006 7919 7726	7000 5928 3304 0702	8469 8263 7882 7430	6813 3535 3080 0654 1777	8346 8261 8032 7759 7360	6337 5237 0622 1686 1686
50	00000	99999	00000	00000	00000	00000	00000
98	864 696 1481 1389	430 319 1108 993	0802 0626 0429 0365 0402	377 254 1137 022 885	715 1568 1420 1370	202 202 063 931 840	204 204 204 204 204 204 204
Š	00000	00000 44440	00000	90000		00000 44400	00000
Ξ̈́	647 677 677 684 684	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0540 0394 0301 0228 0147	030 837 606 608	0308 0236 0270 0191	0790 0794 0651 0520 0410	0302 0294 0255 0169 0052
719		00000		90000			
نو	666 K C O	8 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	908 208 208 208 898	361 173 944 379	6777 3530 3071 0660	242 175 963 701 343	6364 2927 2929 0627 1668
LIF	00000 00000	8 8 K K K	00000	00000	99999	00000	
316	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	32 A 24 A	85 5 5 5 M	### ## C	W 20 40 44	% & & & & & & & & & & & & & & & & & & &	0 4 W 0 W W W W W W W W W W W W W W W W
3	4 2 4 5 E	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	9. 50. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	9 5 9 5 5 7 5 5 5 5 5	£ £ £ 5 £	5 9 9 5 5 8 8 8	94. 63. 7.
HÜH.	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	799 799 798 798 798 798	799 800 800 799 799	735 750 750 750 751	755 749 750 750 750	701 699 699 701	700 700 700 700 699 699
ž X	ප්ප්ප්ස් සුසුසුසුසු	55655 28288	36636 888888	25555 77777	22222 22222	36555 26822	6666666
REY	\$ \$ \$ \$ \$ \$ 5 6 6 5 5	00000	00000 00000 000000	4444	00000	20000	00000 0 44444 4 888888 8
14 14 15	6 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	000 000 000 000 000 000 000 000 000 00	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000 000 000 000 000 000	000 000 010 010 010	014 015 016 017	010 010 010 010 010 010 010 010 010 010

TABLE 2(E) CLERK H)RCRAFT ETA = 0 ETA(T) = +1 1/2

	SIDE F	180. 0 -0.0018 180. 0 -0.0014 180. 0 -0.0017 180. 0 -0.0021 180. 0 -0.0031	180. 0 -0. 0036 180. 0 -0. 0039 180. 0 -0. 0043 180. 0 -0. 0051
	RANG.	1180.0 180.0 180.0 180.0	180.0 180.0 180.0
	ROLL M	0.0020 0.0018 0.0017 0.0020	0.0049 0.0043 0.0043
	Y N N	0.0025 0.0024 0.0024 0.0024	0.0023
	CR055.	0.0018 0.0013 0.0016 0.0020 0.0030	03. 15 - (10. 01 0. 0035 01. 08 - (10. 01 0. 0038 - 00. 99 - (10. 01 0. 0042 - 03. 06 - 00. 01 0. 0050
	ct. 1P		-(10, 01, 10, 10, 10, 10, 10, 10, 10, 10,
	ATRC.	06. 26 05. 25 05. 25 05. 25 06. 19	03, 15 01, 08 -00, 99
	BASE.	0,0020 0,0022 0,0022 0,0024 0,0024	0, 0024 0, 0049 0, 0049
	C.L. 50.	0. 5955 0. 5369 0. 4763 0. 4145 0. 3042	0, 0678 0, 0024 0, 0678 0, 0049 0, 0034 0, 0049
:	HORMAL HXIAL.	-0.0445 -0.0094 -0.0092 -0.0102	-0.0244 -0.0310 -0.0336
	HORMAL	7 -0. 7760 -0. 0415 5 -0. 7376 -0. 0091 9 -0. 6950 -0. 0092 7 -0. 6478 -0. 0152 5 -0. 5545 -0. 0152	-0. 4571 -0. 2615 -0. 0360
	DRAG	0. 1047 0. 0916 0. 0809 0. 0712 0. 0576	0.037
	PITCH.	-0.0582 -0.0471 -0.0405 -0.0365	03.15 0.4551 -0.0294 01.08 0.2607 -0.0217 -00.99 0.0565 -0.0122 -07.06 -0.464 0.0004
	LIFT.	0. 7689 0. 7321 0. 6903 0. 6439 0. 5516	0. 4551 0. 2607 0. 0565
	3 KC 3 Ø.	06. 26 06. 25 05. 24 04. 45	03. 15
	KACH	0.300 0.300 0.300 0.300 0.300	2 2 2 2 2 2 2 3 2 4 2 4
	SER REVN. KACH.	027 0, 449 0, 504 028 0, 449 0, 502 029 0, 450 0, 500 030 0, 452 0, 504 031 0, 452 0, 504	032 0.452 0.500 033 0.450 0.499 034 0.471 0.502

TABLE 2(F) CLERN H)RCRAFT ETA = 0°ETR(T) = +2 1/2°

	ı.	N 0 + 0 0	~ a a m a	ଫୁ କ୍ନମ୍ନ	-049M	MM 4 4 6	4888		
	1 D E	00000	00027 00009 00003 00003	90000	0000	20000	00000	0027 0037 0038 0038 0038	
	Ñ	00000	66666	66666	00000	တ်ဝင်စ်ဝ	00000	00000	
	PKG.	ထုတ်လုံးလုံ တေတာ်လုံးလုံ		ည်ည်ရုံရုံရှိ ဝဝ၈၈၈			9 9 9 9 9		
	æ	4444	-	44444	2 4 4 4 4	88777			
	ור ה	0002 0011 0011 0007	0007 0011 0014 0016 0016	0003 0003 0005 0007 0002	0002 0013 0014 0017	0003 0003 0003 00003	0003 0013 0015 0015	0000	
	20		00000		50000		00000		
	z.	0010 0010 0012 00009 00009	0000 0000 0000 00003	00011 0008 00011 0006	0000 0000 0000 0000 0000	000000000000000000000000000000000000000	0000 0000 0000 0000 0000	40000 40000 40000 60000 60000 60000 60000	
	χ Σ	00000	99999	60000	66666	00000	55555	00000	
	เก๋	4844W	80000 80000	80040	84887 11	11111	4	20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	CROS	88888	0001	0000	000	. 0024 . 0064 . 0037 . 0033	88888	88888 8	
		65000	00000	99999	00000	P C P C P			
	 	66.69	00.01 00.01 00.01 00.01	20.00 20.00 20.00 20.00 20.00	66. 93 66. 94 66. 94 86. 94	26.00 26.00 26.00 26.00 26.00	30 30 00 00 00 00 00 00 00 00 00 00 00 00	36.00.00 36.00.00 36.00.00	
	.		1111		1 1 1	ರವರವರ ಕೃಳಗಳುಗ	25555 25555		
	1 KC.	F 6 5 5 5 5 4 8 8 8 8 8	7. 26 7. 26 7. 28 7. 28 7. 18	07. 42 06. 89 05. 37 05. 32	04, 27 03, 23 04, 42 04, 92 03, 48	*********	સંસંગંગમાં	005. 88 005. 88 005. 88 005. 88	
ы	Œ	MMM4W	00000		1 1	00000	00000		
**	SE E	200 200 200 200 200 200 200 200 200 200	0022 0022 0022 0022 0024	2000 2000 2000 2000 2000	\$022 0022 0022 0023 0023	0022 0024 0024 0024 0022	0022 0024 0024 0039 0039	00018 00018 00024 00020 00022	
# +	Œ	66666	55555	00000	စ်စ်စ်စ်စ်	00000	00000	စ်စ်စ်စ်စ် စံ	
Ê	SQ.	7449 7798 7740 7740 7740	1250 1250 1250 1250 1250 1250 1250 1250	6897 6717 6717 5717 5738	64 4 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	24 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	408 374 374 478	6836 6404 6404 6404 5640	
ETB	당	90000 70000	80000 80000	00000	4 M 4 C C	6 6 6 6 6 6 6 6 6 6	00000 4 m 4 0 0	60000 0	
6	 	8 4 4 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	18 18 18 18 18 18 18 18 18 18 18 18 18 1	140 150 150 150 150 150	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	146 147 192 192 193	7.4 7.79 7.79 7.80 7.80 7.80 7.80 7.80 7.80 7.80 7.80	0	
<u>п</u> С	HX I ?	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	00000	5 5 5 5 5 5 5 5 5 5	20000	2 2 2 2 2	00000	0.034 0.034 0.034 0.034 0.034 0.034	
m.	z	720 :: 371 :: 0008 :: 667 ::	11111	~ <u>~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ </u>		1 1 1 1 1 1 1 1 T	10 W T M 10	*****	
	KORMAL	8 6 6 N N	558 558 558 558 558 558 558 558	84. 8.4. 8.4. 7.6.9. 7.4. 7.4. 7.4. 7.4. 7.4. 7.4. 7.4. 7	447 447 447 447 447 447 447 447 447 447	6666	8 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 8 8 5 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
	=	00000			4 4 10 6 10	64 F 4 E	00000	9449W 8	
	DRAG	168 153 140 140 140 140 140 140 140 140 140	1009 0838 0587 0475	488844	09 4 4 0 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44444 44444 46449	0895 0729 0496 0495	1499 1371 1281 1169 1063	
	_	66666	66666	00000	00000	00000	00000	စ်စ်စ်စ်စ် စံ	
	Ŧ	484 324 360 408 408	463 414 474 478 478 270	227 227 227 329 319	314 211 285 985 304	198 861 861 204 241 266	166 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00424 00424 0044 0044 0044 0044	
	PIT	9 9 9 9 9	44400	0,0,0,0	44000	40444	44000		
		4 9 0 0 0 0	500	9 9 9 4 9	55 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	404k+	8 8 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		
	LIFT	50000 500000 500000 500000 500	0.05	0.83 0.94 0.75 0.75	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0. 821 0. 841 0. 798 0. 769 0. 756	0.00.37	0. 826 0. 800 0. 786 0. 755 0. 751	
	۾	# 8 % B %	, 22,52,23 23,23,24 24,23,24 25,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,24,24 26,2	4 8 W 8 W	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	8 4 7 E K	92494	# # # # # # # # # # # # # # # # # # #	
	180	5 5 5 5 5	2 2 2 2 2 2 3 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	9.5.6.6 9.5.6.6	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.5 0.5 0.5 0.5 0.5	2.	7.55 S. 25 S	
	Ť	22825	ै। क्लान्ट्र	67.5 68.0 68.0 68.0 68.0 68.0 68.0 68.0	881 881 879 679	D =	46 5 2 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		
	KACH	0 8 8 8 8 8 6 8 8 8 8 8 6 5 5 5 5		3	# # # # # :::::::::::::::::::::::::::::		# # # # #		
	ž	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44444 66666 77876	4 4 4 4 4 8 8 8 8 8 8	44 460 764 767 767	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44444 800000 0 77070 0	
	R	66666	66666	00000	66666	00000	66666	00000	
	S. Si	200 200 400 800 800 800 800	007 008 010 010 011	024 024 024 044 044	019 020 021 022 023	026 027 028 029 030	031 032 034 034	03.0 04.1 04.1 04.2 04.2	

TRBLE 2(F) CLERN RIRCRRFI ETR = 0 ETR(T) = +2 1/2

SIDE F	0. 0027 -0. 0010 -0. 0005 -0. 0017 0. 0030	0.0020 0.0017 0.0033 0.0042	0.0018 0.0018 0.0003 0.0013	0.00027 0.00003 0.00043 0.0043	0.0004 0.0001 0.0004 0.0015	0.00041 0.0005 0.0002 0.0044	\$6000 00000 00000 00000 00000 00000 00000 0000
RRWG.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11 11 11 11 11 11 11 11 11 11 11 11 11	1 1 80 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
ROLL M	0.0012 0.0016 0.0013 0.0017 0.0017	0. 0027 0. 0029 0. 0021 0. 0006 0. 0041	0.0022 0.0016 0.0015 0.0017 0.0026	0.0034 0.0042 0.0043 0.0031	0.0022 0.0016 0.0016 0.0017 0.0017	0.0041 0.0046 0.0041 0.0032	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
, ,	0.0003 0.0004 0.0002 0.0006	0. 0001 -0. 0002 -0. 0008 -0. 0008	0, 00004 0, 00004 0, 00003	0.0004 0.0003 0.0003 0.0002 0.0002	0.0003 0.0004 0.0004 0.0004	0.0004 0.0003 0.0003 0.0002	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
CROSS.	-0.0028 0.0009 0.0004 0.0016	-0.0029 -0.0018 -0.0036 -0.0043	-0.0011 -0.0011 -0.0006 -0.0012	-0.0008 -0.0008 -0.0006 -0.0014	0.0007 0.0000 0.0003 0.0014	0.0012 0.0006 0.0001 0.0013	0.0004 0.0004 0.0004 0.0024
SLIP		100.00 100.00 100.00 100.00	60.01 60.01 60.01			(50 00) (60 00) (70 00)	(10.00) (10.00) (10.00) (10.00) (10.00)
A I KC.	03. 27 04. 45 -03. 00 -03. 46	06. 36 05. 36 05. 36 05. 36	03. 29 01. 13 -01. 00 -03. 14	06.88 05.37 05.87 04.39	03. 27 04. 13 -04. 00 -03. 12 07. 36	06.85 05.84 05.84 05.84	03.23 -03.22 -03.23 -03
BASE.	0. 0024 0, 0049 0, 0049 0, 0046 0, 0046	0.0017 0.0018 0.0020 0.0020 0.0020	0.0018 0.0018 0.0018 0.0018 0.0018	0.0020 0.0020 0.0020 0.0020 0.0020	0.0016 0.0020 0.0016 0.0018	0.0019 0.0019 0.0019 0.0018	0.00018
CL 50.	0, 3514 0, 1340 0, 0071 0, 0408 0, 6958	0. 6746 0. 6438 0. 6247 0. 6052 0. 4860	0,3588 0,1136 0,0057 0,0340 0,7013	0, 6774 0, 6488 0, 5615 0, 5672 0, 5672	0.3107 0.0990 0.0052 0.0289 0.6710	0. 6843 0. 6307 0. 6016 0. 5494 0. 4146	0.2807 0.0901 0.0004 0.0234 0.6418 0.6418
RX18L.	-0.0348 -0.0375 -0.0372 -0.0384 -0.0329	-0, 0303 -0, 0294 -0, 0266 -0, 0255 -0, 0244	-0.0246 -0.0338 -0.0338 -0.0270 -0.0270	-0. 0242 -0. 0203 -0. 0476 -0. 0466 -0. 0469	-0. 0209 -0. 0326 -0. 0352 -0. 0272	.0, 0130 -0, 0134 -0, 0137 -0, 0137 -0, 0138	-0.0323 -0.0323 -0.0350 -0.0279 -0.0468
RORHAL	-0. 5961 -0. 3671 -0. 0845 -0. 8459	-0.8313 -0.8110 -0.7977 -0.7841	-0.6017 -0.3382 -0.0759 -0.1867	-0.8320 -0.8432 -0.7947 -0.7584 -0.6890	-0. 3599 -0. 3457 -0. 0727 -0. 4720	-0.8339 -0.8012 -0.7814 -0.7459 -0.6471	-0.3322 -0.3012 -0.0694 -0.4617 -0.9617
DRAG	0. 0708 0. 0468 0. 0376 0. 0409 0. 1433	0, 1312 0, 1206 0, 1100 0, 1007 0, 0796	0.0609 0.0424 0.0363 0.0387 0.1364	0.1126 0.1126 0.1008 0.0898 0.0709	0.0554 0.00409 0.00339 0.00339 0.1300	0. 1204 0. 1039 0. 0931 0. 0633	0.000000000000000000000000000000000000
PITCH.	-0.0896 -0.0662 -0.0481 -0.0368 -0.1042	-0. 1156 -0. 1093 -0. 1014 -0. 0973	-0.0584 -0.0485 -0.0404 -0.0328 -0.1199	-0.0950 -0.0870 -0.0798 -0.0359	-0.0466 -0.0445 -0.0336 -0.0253	-0, 0983 -0, 0583 -0, 0699 -0, 0599	
LIFT.	0. 5929 0. 3661 0. 0851 -0. 2022 0. 8342	0. 8214 0. 8024 0. 7905 0. 7780 0. 7044	0. 5991 0. 3373 0. 0764 -0. 1849 0. 8375	0. 8231 0. 8056 0. 7884 0. 7532 0. 6855	0.5576 0.3149 0.0732 -0.1703	0. 8273 0. 7942 0. 7756 0. 7413 0. 6440	0.3300
JRCJD.	03. 27 04. 15 -01. 00 -03. 16 07. 39	06.85 06.36 05.36 04.86 04.86	03.29 01.13 -01.00 -03.14 07.36	06.88 06.37 05.87 05.39	03. 27 04. 13 -01. 00 -03. 12 07. 36	06. 35 05. 35 05. 84 04. 23	00.420 00
I. KACH.	55 (), 841 55 (), 841 55 (), 840 57 (), 838 53 (), 799	55 0. 804 55 0. 804 55 0. 804 55 0. 800	5 0. 800 5 0. 800 5 0. 800 5 0. 804 4 0. 750	71 0.749 71 0.749 71 0.749 71 0.749 71 0.752	13 0. 748 14 0. 732 14 0. 732 17 0. 749	7 0. 702 7 0. 704 7 0. 700 7 0. 700 7 0. 700	7 0. 704 7 0. 699 7 0. 704 7 0. 700 0 0. 499 9 0. 502
SER REVN	044 0 45 0 45 0 45 0 45 0 45 0 45 0 45	031 0.45 032 0.45 033 0.45 034 0.45	036 0.43 037 0.43 038 0.43 039 0.43	003 0.47 004 0.47 005 0.47 006 0.47	008 0.47 009 0.47 010 0.47 011 0.47	015 0. 457 016 0. 457 017 0. 457 018 0. 457	0210 0.45 0221 0.45 0221 0.45 0231 0.45 027 0.45 027 0.45

TABLE 2(F) CLERN AJRCRAFT ETA = (P ETA(T) = +2 1/2

SIDE F	0.0023 0.0022 0.0013 0.0011	180. 0 0. 0003 180. 0 -0. 0004 180. 0 -0. 0015
RANG.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11 14 80 0 14 80 0 16 0 0
ROLL M	0.0022 0.0020 0.0024 0.0027 0.0027	0.0016 0.0017 0.0018
7 X	0.0000 0.00000 0.00000 0.00000	0. 0004 0. 0002 0. 0003
CROSS.	-0.0026 -0.0023 -0.0020 -0.0012	- (10, 01 -0, 0004 - (10, 01 0, 0003 - (10, 01 0, 0014
5t. 1P.	(10, 01, 10, 10, 10, 10, 10, 10, 10, 10,	. (30. 01 - (30. 01 - (30. 01
ATRC.	06, 24 - ((0, 01 - 05, 73 - ((0, 01 - 05, 24 - ((0, 01 - 05, 24 - ((0, 01 - 03, 14 - ((0,	04.00
BASE.	0.0020 0.0018 0.0020 0.0020 0.0020	0, 0016 0, 0018 0, 0016
CL 50.	0.0 4.0 0.4.0 0.4.0 0.3.0 0.3.0 0.0 0.0 0.0 0.0 0.0 0.0 0	0. 0710 0. 0039 0. 0193
AXTAL.	-0,0087 -0,0084 -0,0094 -0,0141 -0,0141	-0, 0298 -0, 0322 -0, 0262
HORNAL.	-0.7471 -0.6996 -0.6553 -0.5608	-0, 2673 -0, 0632 0, 1411
DRAG	0.0218 0.0799 0.0708 0.0569 0.0476	0. 0364 0. 0328 0. 0352
PITCH.	0.7414 -0.0642 0.6950 -0.0573 0.6514 -0.0534 0.5581 -0.0491 0.4614 -0.0453	04. 07 0. 2666 -0. 0370 -04. 00 0. 0637 -0. 0268 -03. 07 -0. 1395 -0. 0440
JNCJD. LIFT.	0, 7414 0, 6950 0, 6514 0, 55814 0, 55814	0. 2666 0. 0637 -0. 1395
3 NC: 1 D.	06.24 05.23 05.23 04.18 03.14	01. 07 -01. 00 -03. 07
SER REYN. MACH.	028 0, 452 0, 504 029 0, 447 0, 498 030 0, 450 0, 500 031 0, 449 0, 501 032 0, 450 0, 499	033 0.450 0.500 034 0.450 0.500 035 0.449 0.503

TABLE 2(0) CLEAN AIRCRAFT ETA = 0°ETA(T) = +3 4/2

SIDE	9 -0.00001 9 -0.00013 9 -0.0014	0 -0 0004 0 -0 0014 0 -0 0026 0 -0 0057	0.000% -0.00007 -0.000% -0.000%	9 -0.0027 0 -0.0027 0 -0.0036 0 -0.0036	-0.00087 0.00087 -0.00087 -0.00189	0 -0 00082 0 -0 00082 0 -0 0042 0 -0 0058	0 -0 0010 0 -0 0010 0 -0 00110 0 -0 001110 0 -0 001110	
RANG	4444 4444 4444 4444 4444 4444 4444 4444 4444	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4444 6674 6674 6676	4444 460 600 600 600 600 600 600 600 600	4444 6000 9000 9000	00000		
ROLL M	0. 9000 -0. 0003 -0. 0009 -0. 0006 -0. 0008	0.0002 0.0008 0.0010 0.0044 0.0044	0.0044 -0.0003 -0.0009 -0.0007 -0.0002	0.0000 0.0000 0.0009 0.0011	0.0032 0.0012 -0.0007 -0.0006	0. 0001 0. 0009 0. 0011 0. 0009	0.0008 0.0008 0.0008 0.0008 0.0008	
1 1 2 2	0.0017 0.0017 0.0017 0.0016	0.0016 0.0019 0.0027 0.0032	0.0019 0.0019 0.0010 0.0013	0.0022 0.0022 0.0023 0.0030	0, 00047 0, 00068 0, 00144 0, 0019	0.0021 0.0021 0.0021 0.0028	0.0023 0.0023 0.0024 0.0024 0.0024	
CROSS.	0.0004 0.0004 0.0041 0.0041	0.0003 0.0013 0.0027 0.0057 0.0053	-0.0029 0.0006 -0.0007 0.0004 0.0004	0.0026 0.0026 0.0037 0.0033 0.0053	0, 0000 -0, 0026 -0, 0006 0, 0049 0, 0069	0. 0003 0. 0024 0. 0042 0. 0034 0. 0066	0,0003 0,0003 0,0003 0,0003 0,0003 0,0000	
5L 1P.	10.02 100.01 100.01 100.01	10.01 10.02 10.02 10.02 10.02	100.01 100.02 100.01 100.01	(10, 02 (10, 02 (10, 02 (10, 02	10.01 10.01 10.01 10.01	(10.01 (10.01 (10.02 (10.02 (10.02		
ATI€C.	07. 44 06. 89 06. 89 05. 84	04. 25 04. 49 04. 07 03. 20	07. 44 06. 88 05. 36 05. 34	04. 25 04. 25 04. 04 03. 20	05. 48 05. 89 05. 32	04. 23 04. 23 04. 03. 23 03. 20	7.000 0 7.000	
- +3 1/2 BASE.	0.0000 0.0000 0.0000 0.0000 0.0000	0.0088 0.0088 0.0088 0.0088 0.0088	0.0024 0.0024 0.0024 0.0024	0.0022 0.0023 0.0023 0.0024 0.0024	0.0028 0.0028 0.0028 0.0028	0.0024 0.0024 0.0023 0.0023	0.000 0.000	
ETACT) =	0, 7254 0, 6735 0, 5166 0, 5693 0, 5693 0, 5783	0, 4274 0, 3245 0, 4229 0, 0036 0, 0510	0, 6869 0, 6708 0, 6210 0, 5741 0, 5254	0, 4376 0, 3361 0, 1358 0, 0097 0, 0483	0, 6711 0, 6416 0, 6412 0, 5968 0, 5471	0, 4547 0, 3500 0, 1441 0, 0096 0, 0438	0. 5849 0. 6528 0. 6283 0. 5763 0. 5763	
ETA = 0" RXJAL.	-0.0556 -0.0532 -0.0508 -0.0494 -0.0484	-0.0495 -0.0502 -0.0505 -0.0477	-0. 0454 -0. 0455 -0. 0458 -0. 0439	-0.04% -0.044% -0.04% -0.04%	-0.04%6 -0.0400 -0.03%6 -0.03%8	-0. 0384 -0. 0374 -0. 0415 -0. 0375 -0. 0306	-0.0411 -0.0386 -0.0347 -0.0340 -0.0340	
HORMAL	-0.8666 -0.8335 -0.7962 -0.7638	-0.6596 -0.5737 -0.3519 -0.0748	-0. 8422 -0. 8311 -0. 7986 -0. 7665	-0, 5669 -0, 3698 -0, 0987 -0, 0987	-0.8323 -0.6121 -0.8106 -0.7810	-0, 6795 -0, 3950 -0, 3908 -0, 0979 0, 2117	-0.8220 -0.8220 -0.8027 -0.7962 -0.7962	
PRAG	0.1583 0.1583 0.1411 0.1289 0.1188	0, 1007 0, 0843 0, 0592 0, 0486 0, 0564	0. 1566 0. 1566 0. 1375 0. 1248 0. 1138	0.0946 0.0796 0.0547 0.0419	0. 43 24 0. 43 24 0. 42 24 0. 42 24 0. 42 24	0.0913 0.0730 0.0512 0.0379	0, 1300 0, 1300 0, 1269 0, 1079 0, 1059	
P1TCH.	-0.1177 -0.1235 -0.1304 -0.1372 -0.1424	-0.1566 -0.1666 -0.1438 -0.1097 -0.0372	-0.1059 -0.1231 -0.1278 -0.5344 -0.1400	-0. 1406 -0. 1307 -0. 1305 -0. 0982 -0. 0592	-0. 1269 -0. 1071 -0. 1299 -0. 1341 -0. 1394	-0.1432 -0.1313 -0.1313 -0.0634 -0.0633	-0.13307 -0.1340 -0.1340 -0.1363 -0.1363 -0.1363	
) - - - -	0.8517 0.8207 0.7853 0.7546 0.7234	0.6538 0.5698 0.3507 0.0756	0.8289 0.8191 0.7881 0.7577 0.7249	0. 5596 0. 3796 0. 3687 0. 0994 -0. 2202	0. 8193 0. 8010 0. 8008 0. 7726 0. 7397	0, 5947 0, 3796 0, 3796 0, 0964 0, 2097	0.8276 0.8111 0.7835 0.7883 0.7593 0.6893	
INC 1 D.	07. 41 06. 89 06. 36 05. 83 05. 83	04. 25 03. 19 04. 07 -01. 07	07. 41. 06. 36 05. 36 05. 94	04. 26 03. 21 04. 40 -01. 04	07. 38 06. 37 05. 84 05. 32	04. 27 03. 23 04. 42 -01. 03	05. 32 05. 32 05. 32 05. 32	
HACK	0. 899 0. 900 0. 800 0. 898 0. 900	C. 901 C. 901 C. 901 C. 898 C. 898	0. 881 0. 879 0. 884 0. 879 0. 879 0. 880	0. 879 0. 879 0. 864 0. 878 0. 884	7. 764 7. 760 7. 760 7. 750 7. 750 7. 750	C. #61 C. #35 C. #61 C. #61 C. #61	2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
SER REVN.	002 0.458 003 0.458 003 0.458 005 0.458	007 0.455 008 0.455 009 0.455 010 0.453	014 0. 453 015 0. 453 017 0. 453 018 0. 453	059 0.457 020 0.453 021 0.458 022 0.457	026 0. 460 027 0. 457 029 0. 458 030 0. 458	031 0.457 032 0.458 033 0.457 035 0.457	038 0.457 040 0.457 041 0.457 042 0.457 043 0.457	

TABLE 2(0) CLERN HIRCRAFT ETA H OF ETACTO H +3 4/2"

10E F	0034 0054 0052 0062 0062	0023 0023 0003 0004 0018	0031 0036 0046 0064	00028	0034 0034 0058 0058	**************************************	00000000000000000000000000000000000000
v				99999			
RANG	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4 4 4 6 6 6 6 6 0 0 0 0 0	4 4 4 4 4 6 6 6 6 8	4 4 4 4 6 6 6 6 6 6	######################################	4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
ROLL M	0.0009 0.0011 0.0009 0.0013	0.0023 0.0023 0.00023 0.0002	0.0012 0.0012 0.0011 0.0011	0.0033 0.0039 0.0038 0.0026 0.0026	0.0016 0.0011 0.0011 0.0012 0.0013	0.0042 0.0044 0.0027 0.0027	0 0022 0 0041 0 0043 0 0043 0 0024
Y HE	0.0023 0.0033 0.0033 0.0028	0.0026 0.0020 0.0016 0.0015 0.0021	0.0024 0.0027 0.0028 0.0028	0.0022 0.0022 0.0024 0.0024	0.0026 0.0023 0.0023 0.0023	0.0028 0.0028 0.0028 0.0023	######################################
CROSS.	0.0033 0.0040 0.0050 0.0061	0.0028 0.0022 0.0006 0.0003	0, 0030 0, 0035 0, 0045 0, 0063	0,0021 0,0027 0,0041 0,0028 0,0028	0.0037 0.0033 0.0047 0.0057 0.0057	0.0033 0.0033 0.0033 0.0027 0.0027	0.00000 0.00000 0.00000 0.00000 0.00000 0.00000
. I.	. (00, 02 . (00, 02 . (00, 02 . (00, 02 . (00, 02	100.02 100.03 100.03 100.03	-00 02 -00 02 -00 02 -00 02 -00 02	60.00 60.00 60.00 60.00 60.00 60.00	(0.02 (0.02 (0.02 (0.02 (0.03 (0.03		20.00 20.00
A I RC.	03. 23 04. 43 04. 02 -03. 49 07. 37	06. 87 05. 35 05. 35 04. 35	03. 27 04. 13 03. 16 07. 34	06.89 06.80 06.44 06.44	03.25 04.45 -04.02 03.44 07.34	06.83 05.34 05.34 05.34 75.25	03. 24 -04. 40 -03. 42 07. 24 06. 74
BASE.	0.0024 0.0024 0.0020 0.0013	0.0022 0.0023 0.0022 0.0022 0.0022	0.0024 0.0029 0.0020 0.0027	0, 0024 0, 0024 0, 0024 0, 0028	0. 0019 0. 0020 0. 0019 0. 0017 0. 0017	0.0024 0.0024 0.0024 0.0024	0.0024 0.0024 0.0024 0.0024 0.0024
ניר צמ.	0, 3670 0, 1410 0, 0083 0, 0373 0, 6925	0, 6768 0, 6372 0, 6324 0, 6222 0, 5160	0, 3694 0, 5198 0, 0072 0, 0307 0, 7080	0. 6841 0. 6634 0. 6346 0. 6020 0. 4851	0. 324 0. 5052 0. 0064 0. 0252 0. 7083	0.6934 0.6247 0.5247 0.3524 0.4269	0.000000000000000000000000000000000000
AXIAL.	-0, 0342 -0, 0368 -0, 0364 -0, 0289	-0. 0316 -0. 0296 -0. 0256 -0. 0247 -0. 0238	-0. 0259 -0. 0345 -0. 0383 -0. 0283	-0. 02242 -0. 0499 -0. 04689 -0. 0468	-0. 0217 -0. 0337 -0. 0357 -0. 0238	-0.0491 -0.0449 -0.0430 -0.0424 -0.0452	-0.0216 -0.0316 -0.0338 -0.0263 -0.0462 -0.0462
HORHAL	-0, 6090 -0, 3765 -0, 0912 -0, 8954	-0.83294 -0.84294 -0.79494 -0.7253	-0, 6106 -0, 3472 -0, 0847 -0, 1775 -0, 6521	-0.8324 -0.8824 -0.7842 -0.7842	0. 3719 0. 3753 0. 0600 0. 1607	-0.8462 -0.8462 -0.7944 -0.7546	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
DRAG	0. 0707 0. 0464 0. 0467 0. 1453	0, 1331 0, 1224 0, 1096 0, 1009 0, 0803	0.0620 0.0432 0.0358 0.0358	0.1258 0.1127 0.1027 0.0908	0.0550 0.0419 0.0361 0.0383	0, 1211 0, 1070 0, 0936 0, 0643	0.03348 0.0342 0.0364 0.1213 0.1087
PITCH.	-0. 1163 -0. 0938 -0. 0752 -0. 0641 -0. 1217	-0. 1263 -0. 1335 -0. 0951 -0. 1232 -0. 1025	-0.0866 -0.0757 -0.0673 -0.0584	-0. 1224 -0. 1221 -0. 1025 -0. 0942	-0.0748 -0.0715 -0.0620 -0.0507 -0.1247	-0. 1225 -0. 0935 -0. 0980 -0. 0873	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
LIFT.	0, 6059 0, 3756 0, 0918 0, 1935 0, 8322	0. 8228 0. 8107 0. 7951 0. 7888 0. 7888	0.6079 0.3463 0.0953 0.1756 0.8415	0.8272 0.8145 0.7967 0.7760 0.6967	0. 3245 0. 3245 0. 0006 0. 1590 0. 8417	0. 8327 0. 8092 0. 7887 0. 7500 0. 6535	0.00 WW W
JHC10.	03. 25 04. 13 -01. 02 -03. 19	06.87 05.38 05.38 04.38	03. 27 04. 53 -04. 02 -03. 46	06.85 06.84 05.34 04.34	03. 25 04. 44 -04. 02 -03. 44 07. 33	06.83 06.34 05.34 05.35	03. 24 -03. 12 -03. 12 07. 24
. KACH.	57 0.839 55 0.840 57 0.838 55 0.840 67 0.799	67 (1, 801 67 (1, 801 67 (1, 800 67 (1, 800 67 (1, 800	70 0.801 67 0.799 67 0.800 67 0.800 62 0.800	62 0. 731 60 0. 730 60 0. 749 60 0. 749 62 0. 750	60 0.749 62 0.731 62 0.731 63 0.731 49 0.699	9 0. 700 9 0. 700 9 0. 704 9 0. 704 9 0. 700	8889 9889 9899 9899 9899 9899 9899
SER REVM.	0 440 0 440 0 640 0 640 0 640 0 640 0 640	051 0.46 052 0.46 053 0.46 054 0.46	036 0.46 037 0.46 038 0.46 059 0.46	063 0.46 063 0.46 065 0.46 066 0.46	068 0.46 069 0.46 070 0.46 071 0.46 074 0.45	075 0.44 076 0.44 077 0.44 078 0.44	000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

TABLE 2(8) CLEAN HIRCRAFT ETR = 0°E18(T) = +3 1/2°

SIDE F	180.0 -0.0016 180.0 -0.0019 180.0 -0.0023 180.0 -0.0028 180.0 -0.0038	180.0 -0.0038 180.0 -0.0047 180.0 -0.0036
RRNG	4 4 4 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0	180
ROLL H	0.0016 0.0017 0.0024 0.0024	0. 0012 0. 0013 0. 0013
4 3 X	0.0027 0.0027 0.0027 0.0027	0.0025 0.0025 0.0026
CROSS.	0.0018 0.0018 0.0027 0.0027	0.0037 0.0046 0.0055
St. 19.		-(10, 04 -(10, 04 -(10, 04
A 1 RC.	05.72 05.20 04.47 04.47	01, 06
BASE.	0.0022 0.0022 0.0024 0.0024 0.0024	0. 0020 0. 0019 0. 0017
CL 50.	0, 3645 0, 5004 0, 4384 0, 3241 0, 2239	0, 0763
RX I AL.	7551 -0.0000 7120 -0.0079 6659 -0.0055 5723 -0.0143 4754 -0.0202	2772 -0.0299 0728 -0.0327 1318 -0.0267
KORMAL.	-0.7551 -0.7420 -0.6659 -0.5723 -0.4754	-0.2772 -0.0728 0.1318
DRAG	0.0920 0.0810 0.0720 0.0580 0.0484	0, 0370 0, 0332 0, 0334
P.ITCH.	-0.0883 -0.0834 -0.0798 -0.0753	01.06 0.2765 -0.0613 0.0370 -0.01.01 01.073 -0.0506 0.0332 -0.0306 0.0332 -0.03.08 -0.0354 0.03
. LIFT.	0. 7494 0. 7073 0. 6620 0. 5698 0. 4734	0. 2765 0. 0733 -0. 1302
1 HC 1 D	06. 23 05. 72 04. 17 03. 13	04. 06 -04. 04 -03. 08
KHCH.	4 4 9 9 6 4 4 9 9 9 9 9 9 9 9 9 9 9 9 9	c. 500 c. 499 c. 498
SER REYN. KHCH.	088 0, 447 0, 498 049 0. 450 0, 500 0. 450 0. 500 0. 500 0. 500 0. 500 0. 500 0. 450 0. 459 0. 459 0. 459	093 0, 450 094 0, 450 095 0, 447

TABLE 3CA) CLERN AJRCRAFT ETA = -15° ETACT) = +1/2°

FIN 8 - 455-FIN(17) = 444.57		IDE F	0380 0296 0478 0062 0373	0295 0179 0072 0376 0297	0192 0074 0361 0299 0203	0061 0360 0307 0187 0035	0321 0321	0255 0155 0045 0300	0122
FINE 1167 18(1) 1157. P176H DRBG 100HNL N7781. CL58 BRE. N146. SL1P. CR055. VAH K. ROLL K CL58 DRS CL58 CL58		v.		00000	00000	00000	00000	00000	00
Heater H									
FUND HIGH HIGH HIGH HIGH HIGH HIGH HIGH HIG						0.001 0.001 0.001 0.002			
FUN S. LINCH MCD. LIFT. PITCH DRAG HORMAL MXIAL. (CLSA BASE. MINC. SLIF. CR 1.		2					900		
FINE 8 - 455 FIRTY B + 4472 FIRTY BRANCHING NYTH. (LSG. BASE. NIHC. SLIF.) 1. 457 (1.899)		CROSS.		00000	00000	00000	00000	60000	0. 012 0. 003
EVA. HIMCH. JACID. LIFT. PITCH. DRAG HORHMIL. FATAL. CLSG. D. 0448 O. 526. O. 0720 O. 0720 O. 1786 O. 0020 O. 0720 O. 0720 <th></th> <td>St. JP.</td> <td>(10, 03 (10, 03 (10, 02 (10, 03 (10, 03</td> <td></td> <td>5555</td> <td>99999</td> <td>55555</td> <td></td> <td><u>6</u> 6</td>		St. JP.	(10, 03 (10, 03 (10, 02 (10, 03 (10, 03		5555	99999	55555		<u>6</u> 6
REVN. IMPCH. INC.D. LIFT. PITCH. DRAG HORMAL MYIAH. CL59. RFA HORMAL MYIAH. CL59. RFA HORMAL MYIAH. CL59. CL59. RFA LOST CL57. CL57. <th></th> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		-							
REVN. IMCH. JNCJD. LJFT. PJTCH. DRRG HORNGL RVIRL 0.457 (b. 1899) DG. 53 0.7255 0.0719 0.1469 -0.7276 0.0620 0.458 (b. 1894) DG. 53 0.7255 0.0719 0.0784 -0.3744 0.06620 0.458 (b. 1894) DG. 572 0.1459 0.7264 -0.3744 0.06620 0.458 (b. 1894) DG. 272 0.1459 0.0764 -0.3744 0.06620 0.458 (b. 1894) DG. 272 0.1499 0.0764 -0.3744 0.06620 0.458 (b. 1894) DG. 272 0.1499 0.1407 -0.3744 0.0632 0.458 (b. 1894) DG. 274 0.0764 -0.3661 0.0774 -0.3762 0.0570 0.458 (b. 1872) DG. 278 0.1469 0.1407 -0.3661 0.0774 -0.0776 0.458 (b. 1873) DG. 276 0.1340 0.0754 -0.3661 0.0576 0.457 (b. 1840) DG. 276 0.1340 0.0766 -0.3661 0.0774 -0.0766 0.457 (b. 1840) DG. 276 0.1340 0.0576 -0.1469 0.0774 -0.0766 0.457 (b. 1840) DG. 276 <th></th> <td>BASE.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		BASE.							
REVN. HIRCH. JNC.JD. LJFT. PITCH. DRAG HORNMAL RXTRIL. 0.458 (0.898) 0.65.33 0.7285 0.0719 0.1469 0.7376 -0.066 0.458 (0.898) 0.65.31 0.7285 0.1070 0.1376 -0.064 0.458 (0.898) 0.623 0.1787 0.1469 0.1474 0.0643 -0.1296 -0.065 0.453 (0.880) 0.236 0.1787 0.0464 0.1469 0.1524 -0.065 0.453 (0.880) 0.236 0.1787 0.0464 0.1464 -0.0764 -0.1796 0.453 (0.880) 0.236 0.7487 0.0464 0.1504 -0.7274 -0.059 0.453 (0.880) 0.2767 0.1469 0.1504 0.1586 -0.059 -0.056	5"ETRCT)	CL 50.			20 20 20 20 20 20 20 20 20 20 20 20 20 2	22,24,40	00 4 4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0		067
REVN. IMCH. JNCJD. LIFT. PITCH. DRAG IUDRHAL 0.457 0.899 06.53 0.7255 0.0719 0.1469 -0.7376 0.458 0.899 06.53 0.7255 0.1046 0.1070 -0.3736 0.458 0.899 06.53 0.1292 0.1245 0.0643 -0.1296 0.458 0.899 06.237 0.1292 0.1234 0.0643 -0.1296 0.453 0.891 0.1292 0.1294 0.0543 -0.1296 0.453 0.891 0.1394 0.0643 -0.1296 0.453 0.892 0.1489 0.1564 -0.1286 0.453 0.1489 0.1567 0.1383 -0.1286 0.456 0.892 0.1592 0.1383 0.1684 -0.1586 0.457 0.1489 0.2567 0.1383 0.1484 0.2567 -0.1486 0.2665 -0.1486 0.458 0.886 0.1489 0.2692 0.1486 0.1486	# EE	_					ರರದರ		<i>5</i> 5
REVN. HMCH. JNCJD. LIFT. PITCH. DRRG 0.458 0. 899 06. 53 0. 7255 0. 0719 0. 1469 0.458 0. 899 06. 53 0. 7255 0. 1046 0. 1070 0.458 0. 899 06. 53 0. 7255 0. 1046 0. 1046 0.1046 0. 1074 0.458 0. 899 06. 53 0. 7257 0. 1344 0. 0784 0.458 0. 899 0. 25 0. 1292 0. 1344 0. 0643 0.453 0. 880 0. 65 3 0. 7187 0. 0849 0. 1407 0.453 0. 881 0. 65 3 0. 7187 0. 1486 0. 0704 0.453 0. 881 0. 881 0. 381 0. 3832 0. 1486 0. 0704 0.453 0. 881 0. 881 0. 28 0. 1482 0. 1340 0. 0704 0.453 0. 881 0. 881 0. 163 0. 1340 0. 1340 0. 1380 0.453 0. 882 0. 49 0. 5767 0. 1340 0. 0. 0706 0.453 0. 881 0. 881 0. 49 0. 5767 0. 1340 0. 0. 0706 0.458 0. 885 0. 46. 49 0. 5767 0. 1340 0. 0. 000 0.458 0. 881 0. 841 0. 49 0. 5767 0. 1340 0. 0. 000 0.450 0. 841 0. 0. 1340 0. 1340 0. 0. 000 0.451 0. 841 0. 49 0. 542 0. 1486 0. 0. 000 0.452 0. 801 0. 0. 24 0. 3812 0. 1340 0. 0. 000 0.453 0. 800 0. 0. 27 0. 1354 0. 2140 0. 0. 000 0.453 0. 800 0. 0. 27 0. 1354 0. 2140 0. 0. 000 0.453 0. 800 0. 0. 27 0. 3430 0. 1493 0. 1473 0.453 0. 800 0. 0. 27 0. 3430 0. 2440 0. 0. 000 0.454 0. 704 0. 28 0. 2413 0. 2213 0. 0. 000 0.455 0. 700 0. 24 0. 0986 0. 2223 0. 000 <tr< td=""><th>-</th><td>HORMAL</td><td>7376 5744 3754 1296 7302</td><td>00000</td><td>4026 1493 7255 4038</td><td>00000</td><td>0. 7203 0. 5922 0. 0437 0. 0991</td><td>0. 3134 0. 3134 0. 0029 0. 6304 0. 4332</td><td>0. 2621</td></tr<>	-	HORMAL	7376 5744 3754 1296 7302	00000	4026 1493 7255 4038	00000	0. 7203 0. 5922 0. 0437 0. 0991	0. 3134 0. 3134 0. 0029 0. 6304 0. 4332	0. 2621
REVN. IMCH. JNC) D. LIFT. PIT 0. 458 0. 898 06. 53 0. 72555 0. 0 0. 458 0. 898 06. 53 0. 72555 0. 0 0. 458 0. 898 06. 53 0. 7255 0. 0 0. 458 0. 898 06. 25 0. 3720 0. 3 0. 458 0. 898 06. 25 0. 3720 0. 3 0. 458 0. 898 06. 25 0. 7487 0. 0 0. 458 0. 889 06. 25 0. 7487 0. 0 0. 7487 0. 0 0. 453 0. 880 06. 27 0. 3832 0. 0 0. 458 0. 879 06. 34 0. 3482 0. 0 0. 458 0. 869 06. 28 0. 3489 0. 2767 0. 0 0. 458 0. 879 06. 27 0. 1489 0. 2 0. 458 0. 878 0. 876 0. 0 0. 27 0. 1489 0. 2 0. 457 0. 840 0. 0 0. 27 0. 1489 0. 2 0. 457 0. 840 0. 0 0. 3999 0. 2 0. 457 0. 840 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 457 0. 800 0. 0 0. 3999 0. 2 0. 458 0. 800 0. 0 0. 3415 0. 0 0. 458 0. 702 0. 48 0. 33 0. 3415 0. 3 0. 459 0. 6. 35 0. 4497 0. 3499 0. 340 0. 3490 0. 3490 0. 34		DRAG	1469 1070 0784 0643	1024 0734 0604 11383 0976	0707 0565 1304 0937 0665	0542 1243 0867 0601 0518	1171 0774 0574 0484 1110	0545 0545 0463 0619	0492
REVN. HRCH. JNCJ D. L1 0.458 0.899 D6.53 O. 0.458 0.898 D4.46 O. 0.458 0.898 D4.46 O. 0.458 0.898 D6.53 O. 0.460 0.898 D6.25 O. 0.460 0.898 D6.25 O. 0.453 0.880 D6.53 O. 0.453 0.880 D6.25 O. 0.453 0.880 D6.24 O. 0.458 0.859 D6.49 O. 0.458 0.859 D6.49 O. 0.458 0.859 D6.49 O. 0.459 0.890 D6.53 O. 0.459 0.899 D6.53 O. 0.459 0.890 D6.54 O. 0.445 0.793 D6.49 O. 0.445 0.793 D6.49 O. 0.445 0.703 D6.49 O.		_	171 104 134 173		2000 2000 2000 244 248	251 119 181 207 257			N CI
0. 45.5 0. 198.9 0. 45.5 0. 45.5 0. 198.9 0. 45.5 0. 198.9 0. 45.5 0.		-							% B
# 00000 00000 00000 00000 0000 0000 00		1 NC) D.						18881	№ 44
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		ĸ	65666	ခင်းခံခံခံ	4 to 4 to 6	00000	66666	00000	00

TABLE 3(B) CLERN HIRCRAFT ETA = -10 ETR(T) = +1/2"

	4	87779	22072	ទី៥សីសីទី	50.85 5	7.2.2.9.n		MT
	SIDE	. 0034 . 0034 . 00012 . 0001	0011	00010	0029	00017	00013	0003
		80008		00000		00000		0 0
	RANG	1439. 180. 179.	4 4 8 9 0 0 8 4 4 8 9 0 0 8 4 4 9 9 0 0 8 4 9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 4 4 4 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4 4 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	180.0
	بد	00012 0004 0016 0015 0010	00016 0016 0017 0005 0005	0018 0018 0007 0007 0020	0017 0020 0013 0021 0017	0036 0021 0021 0016 0042	0021 0021 0016 0024 0028	0025
	ROLL	00000	00000	00000		00000	00000	6 6
	z i	0015 00015 00005 00004 00015	0004 0004 0006 0015 0013	00003 00014 00014 0000	0000 0000 0000 0000 00003	0000 0000 0000 0000 0000	0001 00001 00003 00003	0002
	7							0 0
	νί Vi	0031 0035 0013 0000 0000	0012 0012 0010 0048 0035	0011 00013 0056 0036 0020	0000 0030 0037 0016 0000	0030 0030 0000 0000 0000 0000	0011 0011 0028 0028	0000
	CRO		90000					00
	<u>.</u> .	55555	88888	88888	40000	84888	01000	2 2
	St. 1P.	55555	ର୍ଗ୍ ଟ ୍ଟ୍ର	55555	£ 5 5 5 5	5555	5555	. 20. - 30.
	ATHC.	7 0 M M 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 8 4 4 4	W W & 4 W	244 W W	4 4 W 4 4 6 B B B B W	8 7 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	. 48 44 44
	æ	9 4 8 0 8	9 9 9 9	80868	0 0 0 0 0	8 2 8 8 8	2888	9 0
*	Š	0018 0017 0014 0012	0014 0013 0011 0016 0014	0013 0014 0014 0013 0013	0011 0013 0014 0010 0010	0012 0014 0014 0006 0006	0012 0011 00014 0016 0016	0011 0010
	E	66666	00000	66666	60060	00000	66666	o o
C 1 M C 1 7	L 50.	3223 3323 3323 0203 3602	3486 1643 1643 1656 1656 1656	2774 0296 5418 3746 1838	0262 3650 4415 1681 0199	3603 3872 3884 3884 3886 3886 3886	3315 1220 0537 4537 2418	0690
נו מ	ני	ರರರದರ	00000	55665	00000	00000	00000	6 6
i.	Æ	0555 0555 0552 0552 0552	0498 0518 0514 0464 0435	0468 0468 0387 0389 0429	0444 0334 0308 0363 0418	0264 0218 0325 0403 0214	0204 0326 0338 0436 0436	0312
<u>.</u>	GX1	2020						ָבְי ה ה
	RHAL	679 1997 1437 193	963 080 710 632 066	238 228 228 2173 312	660 600 600 600 600 600 600 600 600 600	266 753 272 456	3794 3511 1178 6796 4950	900
	FO	\$0000 0000 0000	000000 04460	00000	00000	00000	0,0,0,0,0 8 w 4 6 4	00
	5	1438 1033 0735 0584 1371	0.969 0.696 0.534 1.338 0.917	0633 0483 1241 0890 0619	0461 1203 0826 0544 0432	1126 0716 0488 0415 1061	0658 0477 0409 0898 0581	390
	DRA	99999	00000	00000	04000	0.00 0.00 0.00 0.00 0.00 0.00		0.0
	Ŧ	0067 0341 0630 0972 0059	0803 1117 0159 0159	958 268 304 101	1369 0311 1027 1327 1413	0600 1271 1324 1403 0798	1269 1269 1365 0950	201
	PITCH		66666	00000	00000	5 H H H 5	44464 66666	नं न
		73996 74986 74989 74989	5905 4054 4707 7528 6012	4214 1723 7361 6121 4289	1621 7517 6416 4102 1415	7486 6223 3735 1270 7383	5759 3494 1176 6737 4920	2986 0957
	LJFT	00000	00000 84478	00000	00000	0.0000	0.000 0.000 0.000	0.0
	9	4 4 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 W 4 & W	W 24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	23 22 22	4 4 W 4 4 & 70 W 9 W	2 × 4 × 8	114
	JHCJD	\$ 5 8 8 8	28282	8 5 8 5 8 8 5 8 5 8	55255	5 5 8 8 8	25582	95
	Ŧ	904 200 200 200 878 878	8	2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2	730 730 730 699	5 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	300
	1186	ಕರಕರಕ	ರಕರಕ	ರಕಕಕಕ	ದರದರವ	55555 88584	55555	5 5
	REVE	0.457	0.450 0.450 0.450	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0. 475 0. 470 0. 470 0. 470	44444	4 4 4 4 4 9 7 9 9 4	450
	4	2	0008 0008 0008 0010 0110 0110	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20000 20000 20000 20000	0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	034 0 032 0 033 0 035 0	0 810
	¥1	55 55	55555	2222	2222	8888	2232	E 0

TRBLE 3(C) CLERK RIRCRAFT ETR m -5° ETR(T) m +1/2°

SIDE F	0.0049 0.0018 0.0018 0.0052	0.0039 0.0004 0.0004 0.0049	0.0002 0.0002 0.0046 0.0036	0, 0008 0, 0034 0, 0027 0, 0013	0.0003 0.0023 0.0003 0.0003	0.00019 0.0007 0.00084 0.00084	0. 000% 0. 000%
RANG	179.9 180.0 180.0 179.9	180.0 180.0 179.9 180.0	180.0 180.0 179.9 180.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	180.0
ROLL M	0.0011 0.0005 0.0016 0.0014 0.0008	0.0002 0.0016 0.0014 -0.0004 0.0004	0.0018 0.0017 -0.0003 0.0006	0.0016 0.0022 0.0015 0.0020 0.0017	0.0043 0.0021 0.0020 0.0016	0.0027 0.0019 0.0016 0.0022 0.0028	0. 0021 0. 0018
Y WEY	-0.0004 -0.0006 -0.0004 -0.0004	-0, 00003 -0, 00004 -0, 0013 -0, 0004	-0.0008 -0.0001 -0.0014 -0.0010 0.0002	-0, 0002 -0, 0040 -0, 0006 -0, 0002 -0, 0001	0.0000 -0.0004 -0.0002 -0.0002	0. 0000 0. 0000 0. 00002 0. 0002	0.0004
CR0SS.	-0.0035 -0.0049 -0.0062 -0.0062	-0.00040 -0.0003 -0.00050 -0.0050	-0. 0024 -0. 0003 -0. 0037 -0. 0037	-0.00099 -0.0028 -0.0044 -0.006	-0.0006 -0.0026 -0.0040 -0.0004	-0.0008 -0.0008 -0.0009 -0.00025	-0. 00 06 0. 0004
St. 1P.	00 00 00 00 00 00 00 00 00	60.00 60.00 60.00 60.00 60.00 60.00 60.00	(10, 00 (10, 00 (10, 00 (10, 00 (10, 01	30.00 30.00 30.00 30.00 10.00	30.00 30.00 30.00 30.00 30.00	(30, 01 (30, 01 (30, 01 (30, 01 (30, 01	-(10. 04 (10. 00
ATMC.	06. 34 000. 34 000. 34 000. 34	04. 25 06. 24 06. 44 04. 44	02.23 00.46 06.45 02.38	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.4.4 0.00 0.8.4 0.00 0.8.4 0.00 0.00	04.22 00.03 04.23 04.23 04.23 04.23	02. 15 00. 08
BASE.	0.0022 0.0022 0.0043 0.0043 0.0050	0.0018 0.0018 0.0016 0.0018	0, 0017 0, 0015 0, 0018 0, 0018 0, 0016	0.0015 0.0016 0.0018 0.0018	0.0016 0.0016 0.0014 0.0014	0.0016 0.0013 0.0014 0.0014 0.0014	0. 0016 0. 0015
CL SQ.	0, 5081 0, 3816 0, 1744 0, 0279 0, 5943	0, 3773 0, 4839 0, 0375 0, 6016 0, 3906	0, 1995 0, 0388 0, 5760 0, 4080	0, 0343 0, 4430 0, 4430 0, 1885 0, 0280	0, 5909 0, 4172 0, 1573 0, 0236 0, 5764	0, 3572 0, 1383 0, 0204 0, 4688 0, 2663	0, 1064 0, 0152
AX I AL.	-0, 0518 -0, 0518 -0, 0508 -0, 0508 -0, 0550	.0.0452 .0.0454 .0.0465 .0.0455 .0.0425	.0, 0424 .0, 0424 .0, 0384 .0, 0384 .0, 0354	-0, 0392 -0, 0302 -0, 0266 -0, 0311	-0, 0226 -0, 0378 -0, 0298 -0, 0370	-0.0167 -0.0289 -0.0361 -0.0402 -0.0465	-0, 0277
NORMAL	-0. 7890 -0. 6238 -0. 4203 -0. 4675	-0.6198 -0.1942 -0.7857 -0.7857 -0.6301	-0. 4492 -0. 1976 -0. 7683 -0. 6437	-0, 1861 -0, 7794 -0, 6715 -0, 4361 -0, 1680	.0. 43464 .0. 3987 .0. 43484 .0. 4348	-0. 6010 -0. 3735 -0. 1433 -0. 7049	-0, 3276 -
DRAG	0.1418 0.1009 0.0591 0.0532	0.0940 0.0660 0.0483 0.1321	0.0620 0.0443 0.0264 0.0864	0.0412 0.1190 0.0801 0.0501	0. 1108 0. 0691 0. 0469 0. 0388	0.0637 0.0449 0.0377 0.0892	0.0416 0.0362
PITCH.	-0.0733 -0.0397 -0.0453 0.0446	-0. 0224 -0. 0003 0. 0286 -0. 0479 -0. 0094	0. 0166 0. 0437 0. 0080 0. 0034 0. 0323	0.0568 -0.0182 0.0296 0.0550 0.0528	-0 0005 0. 0532 0. 0570 0. 0638 0. 0136	0.0522 0.0552 0.0637 0.0411	0.0522
LIFT.	0. 7779 0. 6178 0. 4178 0. 1673 0. 7709	0. 6143 0. 4290 0. 1940 0. 7756 0. 6250	0. 4469 0. 1974 0. 7590 0. 6388 0. 4544	0. 1858 0. 7705 0. 6672 0. 4343 0. 1678	0, 7688 0, 6460 0, 3970 0, 1540 0, 7592	0. 5977 0. 3719 0. 1431 0. 6992 0. 5162	0. 3264 0. 1237
3 MC 3 D.	06. 42 04. 34 00. 34 00. 12 06. 42	04, 35 02, 26 00, 14 06, 43	00. 26 06. 16 06. 38 02. 38	00. 16 06. 44 04. 42 02. 31	96 92 92 96 96 96 96 96	04.33 02.22 00.12 06.26	02. 15 00. 08
VW. BRCH.	458 0.903 448 0.903 448 0.900 458 0.900 458 0.900	44% (), 881 44% (), 882 44% (), 880 4%% (), 864 4%% (), 864	435 (), 864 432 (), 862 445 (), 840 445 (), 838 447 (), 841	447 0.841 462 0.801 462 0.799 462 0.800 462 0.800	442 0. 732 440 0. 750 440 0. 750 442 0. 750 419 0. 700	419 (i. 701 422 (i. 699 419 (i. 700 437 (i. 499	437 0.500
SER REVE	20000 4 M 7 S 4 20000 20000	0.02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0139 028 0 0 023 0 0 024 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000	038 0

TABLE 3(D)
CLERN RINCRAFT
ETR = 0°ETR(T) = +1/2°

SIDE F	0.0032 0.0033 0.0036 0.0041 0.0042	0. 0036 0. 0025 0. 0016 0. 0005	0.0054 0.0049 0.0040	0.0031 0.0022 0.0017 0.0005	0.0036 0.0057 0.0048 0.0048	0.0039 0.0023 0.0004 0.0000	0.00022 0.00044 0.00464 0.0033
RANG.	274 274 274 274 274 274 274 274 274 274	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	180.0 179.9 179.9 179.9 179.9	180.0 180.0 180.0 180.0	180.0 180.0 179.9 179.9	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1180.0 14790.0 18790.0 1800.0
ROLL M	-0. 0002 -0. 0003 -0. 0040 -0. 0005 -0. 0005	0.0004 0.0011 0.0015 0.0017 0.0017	0.0008 -0.0002 -0.0008 -0.0004 -0.0004	0.0002 0.0013 0.0016 0.0018 0.0018	0.00034 -0.00033 -0.00053 -0.0005	0.0004 0.0043 0.0043 0.0048	0.00020 0.00020 0.00020 0.00020 0.0004
ž Ž	-0.0003 -0.0009 -0.0044 -0.0044 -0.0044	-0.0010 -0.0010 -0.0001 -0.0001	-0, 0044 -0, 0008 -0, 0044 -0, 0043	-0.0044 -0.0009 -0.0006 -0.0002 0.0003	-0.0012 -0.0014 -0.0014 -0.0014	-0. 0011 -0. 0009 0. 0002 0. 0000	-0.00040 -0.00040 -0.00040 -0.00440 -0.00440
CROSS.	-0.0033 -0.0034 -0.0039 -0.0042	-0.0040 -0.0026 -0.0017 0.0004 0.0004	-0.0055 -0.0034 -0.0050 -0.0041 -0.0043	-0,0032 -0.0023 -0.0018 -0.0006	-0.0037 -0.0058 -0.0046 -0.0045	-0.0040 -0.0024 -0.0002 0.0049	0.000 00 00 00 00 00 00 00 00 00 00 00 0
St.1P.	(10.00 (10.00 (10.00 (10.00 (10.00	60.00 60.00 60.00 60.00 60.00	26. 00 26. 00 26. 00 26. 00	60.00 60.00 60.00 60.00 60.00	6.00.00 6.00.00 6.00.00 6.00.00	90.00 (60.00 (60.01	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PINC.	07. 42 06. 90 06. 37 05. 83 05. 83	04. 29 03. 24 04. 42 -04. 04	07. 44 06. 90 06. 38 05. 86	04.26 03.26 00.26 00.99	07. 44 06. 94 06. 39 05. 87	04. 32 03. 28 04. 47 00. 98 -03. 44	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
BASE.	0.0024 0.0023 0.0022 0.0022	0.0021 0.0021 0.0013 0.0017 0.0017	0.0023 0.0023 0.0023 0.0023 0.0023	0.0020 0.0018 0.0017 0.0016 0.0016	0.0020 0.0019 0.0020 0.0020 0.0020	0.0019 0.0020 0.0045 0.0046	0.0000000000000000000000000000000000000
CLSQ.	0, 7424 0, 6894 0, 6898 0, 3699 0, 3195	0, 4098 0, 2972 0, 1013 0, 0024 0, 0639	0, 6977 0, 6775 0, 6233 0, 5668 0, 5468	0, 4098 0, 3033 0, 1158 0, 0053 0, 0608	0, 6835 0, 6604 0, 6307 0, 5787 0, 5787	0, 4221 0, 3152 0, 1247 0, 0052 0, 0543	0.000000000000000000000000000000000000
AXIAL.	-0, 0536 -0, 0528 -0, 0548 -0, 0500	-0.0492 -0.0504 -0.0502 -0.0466	-0, 0464 -0, 0464 -0, 0443 -0, 0437	-0.04% -0.04% -0.04% -0.044% -0.044%	-0, 0439 -0, 0411 -0, 0403 -0, 0395 -0, 0389	-0.0367 -0.0401 -0.0423 -0.0382	-0.0393 -0.0393 -0.0359 -0.0346 -0.0343
RORMAL	-0.8762 -0.8432 -0.8047 -0.7643	-0, 6460 -0, 3492 -0, 0488	-0.8352 -0.7998 -0.7617 -0.7521 -0.7521	0.000	0,8396 -0,8240 -0,7692 -0,7692	0.6547 0.3650 0.3544 0.0724 0.2734	0.000 0.000
DRAG	0.1584 0.1560 0.1580 0.1298	0.0935 0.0831 0.0583 0.0474	0, 1599 - 0, 1485 - 0, 1233 - 0, 120 -	0.0932 0.0767 0.0559 0.0416	0.1538 0.1418 0.1418 0.1200 0.1089	0.0878 - 0.0743 - 0.0511 - 0.0386 - 0.0454	0.1478 0.1376 0.1267 0.1053
P1TCH.	-0.1186 -0.1193 -0.1237 -0.1221 -0.1181	-0.1081 -0.0991 -0.0756 -0.0372	-0.0773 -0.1143 -0.1135 -0.1100	-0.0893 -0.0780 -0.0584 -0.0290 0.0414	-0. 1075 -0. 0919 -0. 1060 -0. 1012 -0. 0918	-0. 0743 -0. 0630 -0. 0426 -0. 0462 0. 0065	10.00000000000000000000000000000000000
LIFT.	0.8615 0.8304 0.7936 0.7549 0.7208	0, 6402 0, 3453 0, 3484 0, 0495	0.8232 0.7896 0.7896 0.7529 0.7447	0. 6402 0. 3509 0. 3405 0. 0733	0.8268 0.8427 0.7942 0.7608 0.7236	0.56498 0.3616 0.3533 0.0727	0.8497 0.7920 0.7722 0.7722 0.7361
) RC) D.	07. 42 06. 90 06. 37 05. 85 05. 85	04. 24 03. 24 04. 24 04. 62 03. 15	05. 44 06. 90 06. 38 05. 86 05. 34	04.34 03.26 04.45 -00.99	07. 41 06. 91 06. 39 05. 37 05. 35	04, 32 03, 28 01, 17 -00, 98 -03, 14	0.07. 34 0.05. 34 0.05. 34 0.05. 34 0.05. 34
. NACH.	7 0 896 9 0. 900 9 0. 901 0 901	2 C 889 7 C 900 9 C 900 7 C 900	3 C. 879 C C. 88C C C. 876 C C. 681 C C. 661	0 0. 879 0 0. 880 0 0. 880 0 0. 880 0 0. 879	2 0. 864 2 0. 864 2 0. 864 2 0. 862 2 0. 862	0 0.859 2 0.860 2 0.860 2 0.860 0 0.859	25 0 840 25 0 840 25 0 840 2 0 840 2 0 840 2 840 2 840
SER REVN.	202 0 449 203 0 449 205 0 449 205 0 444	007 0.450 008 0.445 009 0.445 010 0.445	014 0, 453 015 0, 450 016 0, 452 017 0, 450 018 0, 450	0139 0, 450 020 0, 450 021 0, 450 022 0, 450 023 0, 450	026 0.48 027 0.44 028 0.44 029 0.48 030 0.45	034 0, 450 032 0, 452 033 0, 452 034 0, 452 035 0, 450	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

TABLE 3(D) CLERN HJRCRRFT ETR = 0°ETR(T) = +1/2°

SIDE F	0.0024 0.0012 0.0003 0.0020 0.0031	0.0019 0.0032 0.0033 0.0033	0.0022 0.0013 0.0010 0.0000	0.0015 0.0005 0.0017 0.0010	0.00021 0.0013 0.0006 0.0010	0.0028 0.0020 0.0042 0.0046	0.0018 0.0018 0.0014 0.0001	0. 0026
RANG.	190, 0 190, 0 190, 0 180, 0	180.0 180.0 180.0 180.0	180.0 180.0 180.0 180.0	180.0 180.0 180.0 180.0	180. 0 180. 0 180. 0 180. 0	180.0 180.0 180.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	190.0
ROLL #	0.0015 0.0018 0.0017 0.0020 0.0026	0.0025 0.0029 0.0031 0.0018 0.0006	0.0012 0.0023 0.0017 0.0016	0.0046 0.0046 0.0046 0.0043	0.0022 0.0023 0.0017 0.0017 0.0010	0. 0036 0. 0045 0. 0042 0. 0032	0.0029 0.0028 0.0017 0.0017 0.0020	0. 0027
Y MEY	-0, 0010 -0, 0002 -0, 0000 -0, 0000	-0, 0007 -0, 0005 -0, 0010 -0, 0012	-0, 00008 -0, 00004 -0, 00006 -0, 00002	-0. 0003 -0. 0004 -0. 0004 -0. 0004	-0.0006 0.0004 0.0000 -0.0005 -0.0005	-0.0003 0.0001 0.0002 -0.0001	-0. 0002 -0. 0006 -0. 0004 -0. 0003	0. 0002
CR055.	-0.0022 -0.0013 -0.0004 -0.0019	-0.0020 -0.0033 -0.0034 -0.0034	-0.0023 -0.0016 -0.0011 -0.0001	-0.0016 -0.0006 -0.0018 -0.0011	-0.0022 -0.0014 -0.0007 -0.0001 0.0008	-0.0021 -0.0021 -0.0043 -0.0047 -0.0046	-0.0020 -0.0013 -0.0000 0.0000	-0. 0027
St. 1P.	\$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00	60.00 60.00 60.00 60.00 60.00 60.00	60.00 60.00 60.00 60.00 60.00	90.000	(10, 00 (10, 00 (10, 00 (10, 00 (10, 00	60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00	6.0.00 6.0.00 6.0.00 6.0.00 6.0.00 6	(10. 0 1
A1RC.	03. 30 01. 18 -00. 97 -03. 14	07, 39 06, 88 06, 30 05, 90 03, 39	04. 36 03. 32 04. 47 -00. 97	07. 39 06. 89 06. 38 05. 88	04, 35 03, 29 01, 15 -00, 97	07. 36 06. 88 06. 37 05. 86	04, 34 03, 255 06, 34 100, 98	07, 27
BASE	0.0015 0.0015 0.0015 0.0013	0, 0017 0, 0018 0, 0017 0, 0018 0, 0018	0,0018 0,0017 0,0013 0,0013	0, 0015 0, 0015 0, 0017 0, 0017 0, 0017	0, 0015 0, 0016 0, 0016 0, 0018	0, 0016 0, 0018 0, 0018 0, 0016	0,0017 0,0017 0,0018 0,0013 0,0013	0. 0025
CLSQ.	0, 3326 0, 1206 0, 0044 0, 0488 0, 6719	0, 6715 0, 6339 0, 6324 0, 5920 0, 5782	0, 4733 0, 3417 0, 1025 0, 0034 0, 0406	0, 6759 0, 6346 0, 6340 0, 5974 0, 5630	0, 4449 0, 2947 0, 0871 0, 0029 0, 0350	0, 6637 0, 6354 0, 6117 0, 5730 0, 5173	0.3885 0.2595 0.0781 0.0024 0.0316	0. 6088
RXIAL.	-0. 0360 -0. 0381 -0. 0377 -0. 0297 -0. 0389	-0, 0334 -0, 0302 -0, 0290 -0, 0270	-0, 0249 -0, 0258 -0, 0338 -0, 0370 -0, 0284	-0, 0272 -0, 0232 -0, 0244 -6, 0493 -0, 0463	.0. 0266 .0. 0221 .0. 0338 .0. 0351	-0, 0228 -0, 0477 -0, 0458 -0, 0433	-0, 0453 -0, 0241 -0, 0324 -0, 0354 -0, 0275	n. 0349
RORHAL	-0. 3801 -0. 3485 -0. 0661 0. 2231 -0. 8320	-0, 8311 -0, 8186 -0, 8038 -0, 7766 -0, 7664	-0, 6922 -0, 5873 -0, 3244 -0, 0586	-0, 8330 -0, 8056 -0, 8020 -0, 7594	-0, 6705 -0, 7454 -0, 2961 -0, 0543	-0, 8248 -0, 8054 -0, 7891 -0, 7627 -0, 7238	0.626 0.2416 0.2416 0.0490 0.495	0. 7869
DRAG	0. 0711 · 0. 0468 · 0. 0380 · 0. 0431 · 0. 1476 · 0.	0. 1299 0. 1299 0. 1099 0. 1095	0.0793 0.0645 0.0448 0.0373	0.1337 - 0.1212 - 0.1108 - 0.1088 -	0,0691 0,0549 0,0411 0,0354	0, 1299 0, 1157 0, 1050 0, 0930	0,0640 0,0516 0,0391 0,0355 0,0353	0, 1167 -
PITCH.	0. 0487 0. 0253 0. 0092 0. 0041 0. 1083	0. 0996 0. 0986 0. 0882 0. 0496 0. 0579	0. 0359 0. 0212 0. 0108 0. 0026 0. 0071	0. 0756 0. 0502 0. 0631 0. 0487 0. 0321	0. 0113 0. 0089 0. 0078 0. 0006 0. 0120	0. 0742 0. 0446 0. 0438 0. 0330 0. 0217	0.0111 0.0102 0.0067 0.0024 0.0150	0.0525
LIFT.	0. 3425 - 0. 3425 - 0. 0667 - 0. 2211	0.8195 - 0.8087 - 0.7694 - 0.7694 -	0. 6880 - 0. 5846 - 0. 3203 - 0. 0591 - 0. 2018	0. 8222 - 0. 7967 - 0. 7944 - 0. 7730 -	0.5671 - 0.5430 - 0.2952 - 0.0548	0.8147 - 0.7972 - 0.7821 - 0.7570 -	0.6834 0.5093 0.2796 0.0500 0.1782	0. 7803 -
J MC J D.	03, 30 01, 18 -00, 97 -03, 14 ~	07, 39 06, 88 06, 38 05, 90	04. 36 03. 32 01. 17 -00. 97	07, 39 06, 89 06, 38 05, 88	04. 35 03. 29 04. 45 00. 97	07.36 06.98 06.37 05.86	04.31 03.25 01.14 -00.98	07. 27
ийсн.	0. 840 0. 839 0. 841 0. 839 0. 839	0. 799 0. 799 0. 796 0. 800	0. 604 0. 604 0. 799 0. 804	G. 750 G. 750 G. 750 G. 750	0. 749 0. 749 0. 730 0. 730 0. 749	(c. 699 (c. 701 (c. 701 (c. 702 (c. 699	0. 700 0. 700 0. 700 0. 700 0. 700	0. 301
SER REVN.	044 0.449 045 0.445 045 0.447 047 0.449	052 (), 444 052 (), 445 053 (), 445 054 (), 445 055 (), 445	056 0, 444 057 0, 444 058 0, 444 059 0, 445 060 0, 445	063 0, 442 064 0, 442 065 0, 440 066 0, 442	068 0.442 069 0.442 070 0.442 071 0.442	076 0. 440 (177 0. 442 (178 0. 442 (179 0. 442	063 0.442 063 0.442 063 0.442 084 0.442 085 0.442	086 0, 437
•	-		-			-		_

TABLE 3KD) CLERN RIRCRAFT ETR R 0°ETR(T) = +1/2°

SIDE F	0.0026 0.0025 0.0026 0.0019	180. 0 0, 0011 180. 0 0, 0006 180. 0 -0, 0001 180. 0 -0, 0001
RANG	180.0 180.0 180.0 180.0	180.0 180.0 180.0
ROLL M	0.0023 0.0024 0.0023 0.0024 0.0024	0.0026 0.0019 0.0019 0.0022
Y XX	0.0002 0.0003 0.0001 0.0001	0. 0000 0. 0000 0. 0000 -0. 0002
CROSS.	-0.0027 -0.0026 -0.0027 -0.0020	(10. 030. 0011 (10. 000. 0007 (10. 01. 0. 0000 (10. 00. 0. 0006
St. 1F.	06. 26(10. 01 06. 26(10. 01 05. 24(10. 01 05. 23(10. 01 04. 19(10. 01	-(10. 01 (10. 00 -(10. 01 (10. 00
ATRC.		03. 16 01. 09 -00. 98 -03. 05
BASE.	0.0020 0.0020 0.0020 0.0021 0.0021	0,0018 0,0017 0,0015 0,0014
CL.50.	0, 9676 0, 9153 0, 4521 0, 2974 0, 2869	0, 1932 0, 0606 0, 0018 0, 0248
RX J.A.L.	-0, 0402 -0, 0065 -0, 0087 -0, 0099 -0, 0449	4440 -0, 0209 2472 -0, 0308 0438 -0, 0324 1593 -0, 0270
HORMAL	-0.7602 -0.7234 -0.6770 -0.5386	-0.2472 -0.2472 -0.0438 0.1593
DRAG NO	0, 1016 0, 0893 0, 0784 0, 0697 0, 0560	0, 0472 0, 0371 0, 0331 0, 0368
PITCH.	-0.0370 -0.0270 -0.0221 -0.0188	-0.0117 -0.0045 0.0058 0.0187
LIFT	0, 7534 0, 7178 0, 6725 0, 6305 0, 5358	03. 16 0. 4420 01. 09. 01. 09 0. 2464 -00. 98 0. 0443 -03. 05 -0. 1577
THETO. LIFT.	06. 26 05. 24 05. 24 05. 23	03. 16 01. 09 -00. 96 -03. 05
иясн.	089 0, 437 0, 501 090 0, 437 0, 501 091 0, 437 0, 501 092 0, 434 0, 500 093 0, 437 0, 500	094 0, 437 0, 502 095 0, 437 0, 502 096 0, 437 0, 500 097 0, 437 0, 500
SER REYN, 114CH.	9 0, 437 0 0, 437 1 0, 437 2 0, 434 8 0, 437	5 0, 437 5 0, 437 5 0, 437 0 , 437
135	180 180 180 180 180 180 180 180 180 180	\$6.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5

TABLE 3(E) CLEAN AJRCRAFT TA = +5°ETACT) = +1.7

NATRAL CLSG BMSE NATUC SLIP CROSS VAN H ROLL RANG RANG CLSG BMSE RANG CLSG CL		. SIDE F	9 -0.0007 0 -0.0022 0 -0.0036 0 -0.0044	9 -0, 0019 0 -0, 0049 0 -0, 0044 0 -0, 0004	0 -0. 0042 9 0. 00034 0 -0. 0042 0 -0. 0042	0 -0. 00048 0 -0. 00048 0 -0. 0004	0 -0, 0025 0 -0, 0025 0 -0, 0040 0 -0, 0046	0 -0.0036 0 -0.0036 0 -0.0046 0 -0.0020 0 -0.0020
Fig. 1.47 110 11 11 11 11 11 11		•	4444 9664 9000 9000	179. 180. 179. 180.	180. 180. 180.	4 4 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
HETH REPLY NUCLEAR THOSE OF THE PERCENTINE REPLY HETHER REPLY HETHER STATES OF THE STA		110	000	00000	9000	900	4440	002
FITA = +5° ETR(T) = +14/2" FITCH DRNG HORMAL RMTAL CLSG BMSE NINC SLIP CR		3	002	0000	900	00000	0005	
ETR = +5°ETR(T) = +472" REYN. 196T. 196T. 0.17T. PITCH. DRAG 100NHAL RYINL. (LISG. BASE. NINC. 5LI C. 1447 0.502 0.6.3 6.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		ROS			0000		90000	004
FIRE # +5° ETRCT 1 FILCE		_	99999	5 6 6 6 6 6 6 6 6 6	58888	56888	55853	55555 5
REVN.		-			40 M 68 44		WWAOW	84088 4
ETA = +5°ETA (147)	+4/2	Ž.	2002		0004	20000	88888	
REYN. HIRCH. JUCID. LIFT. PITCH. DRRG RORNAL RRIAL. 0. 447 0. 802 0. 7897 -0. 1374 0. 1407 -0. 6604 -0. 0438 0. 444 0. 802 0. 7837 -0. 1374 0. 1407 -0. 6604 -0. 0438 0. 447 0. 802 0. 233 0. 4622 -0. 1539 0. 0513 -0. 4647 -0. 0432 0. 447 0. 801 0.0. 33 0. 7827 -0. 1417 0. 1330 -0. 6639 -0. 1437 0. 1430 -0. 6632 -0. 0432 0. 442 0. 801 0.0. 33 0. 7827 -0. 1437 0. 1350 -0. 6349 -0. 1350 -0. 6329 -0. 1350 -0. 6329 -0. 1350 -0. 6329 -0. 1350 -0. 1350 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1437 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 1433 -0. 143	ETACT	16	E 4 14 C C	4 00 00 4 W 0 00 4 00 W V 10 4 10	SCEAU	00000 0000 04464 4464	638 638 634 634	емвыя м
REVN. IMCH. JMCJD. LIFT. PITCH. DRAG RORMAL 0. 447 0. 802 06.346 -0. 1374 0. 1407 -0. 6604 0. 447 0. 802 06.346 -0. 1574 0. 1407 -0. 6604 0. 447 0. 802 02. 13 0. 6546 -0. 1594 0. 0543 -0. 4649 0. 447 0. 901 0.0 0. 787 -0. 1417 0. 1350 -0. 2149 0. 447 0. 802 0. 248 -0. 1599 0. 0543 -0. 6652 0. 447 0. 802 0. 7927 -0. 1417 0. 1350 -0. 2449 0. 442 0. 803 0. 7927 -0. 1417 0. 1350 -0. 6658 0. 442 0. 803 0. 7425 -0. 1431 0. 0439 -0. 1340 -0. 6658 0. 442 0. 803 0. 803 -0. 1341 0. 0425 -0. 1431 0. 0425 -0. 1431 0. 440 0. 804 0. 474 0. 470 0. 474 0. 474 0. 474 0. 474 0. 474	# # # # # # # # # # # # # # # # # # #	244	0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 0.4	-0.0435 -0.0448 -0.0438 -0.0397 -0.0364	0, 033 0, 033 0, 033 0, 033	ರರ್ಥರ		0.000 0.000 0.000 0.000 0.000 0.000 0.000
REVN. JHCH. JHCJD. LIFT. PITCH. DRAG 0. 447 0. 902 06.36 0. 7897 -0. 1374 0. 1407 0. 447 0. 802 06.36 0. 7897 -0. 1374 0. 1407 0. 444 0. 802 06.25 0. 6548 -0. 1599 0. 0943 0. 447 0. 902 07. 13 0. 4622 -0. 1429 0. 0513 0. 447 0. 801 07. 13 0. 6599 -0. 1417 0. 1350 0. 447 0. 802 0. 7927 -0. 1415 0. 0439 0. 447 0. 802 0. 774 -0. 1437 0. 0436 0. 447 0. 802 0. 6745 -0. 1431 0. 0436 0. 447 0. 803 0. 8039 -0. 1431 0. 0436 0. 447 0. 804 0. 6745 -0. 1431 0. 0436 0. 434 0. 804 0. 6745 -0. 1431 0. 0426 0. 434 0. 804 0. 6745 -0. 1431 0. 0426 0. 434 0. 804 <td></td> <td>NORMAL</td> <td>0. 860 0. 660 0. 464 0. 214 0. 802</td> <td>0. 6652 0. 4796 0. 2398 0. 8133 0. 6793</td> <td>0. 2393 0. 2393 0. 8476 0. 6942 0. 4997</td> <td>2262 8404 7193 2116</td> <td>0. 8192 0. 6931 0. 4415 0. 1974 0. 8141</td> <td>6503 4197 7816 7816 7816</td>		NORMAL	0. 860 0. 660 0. 464 0. 214 0. 802	0. 6652 0. 4796 0. 2398 0. 8133 0. 6793	0. 2393 0. 2393 0. 8476 0. 6942 0. 4997	2262 8404 7193 2116	0. 8192 0. 6931 0. 4415 0. 1974 0. 8141	6503 4197 7816 7816 7816
REVN. HACH. JAC1D. LIFT. P1 0. 447 0. 902 06. 36 0. 7897 -0. 0. 444 0. 892 04. 25 0. 6548 -0. 0. 447 0. 902 02. 13 0. 4622 -0. 0. 447 0. 902 02. 13 0. 4622 -0. 0. 447 0. 904 02. 13 0. 4622 -0. 0. 447 0. 881 06. 35 0. 7927 -0. 0. 447 0. 882 04. 25 0. 6745 -0. 0. 447 0. 882 04. 25 0. 6745 -0. 0. 447 0. 882 04. 25 0. 6745 -0. 0. 447 0. 882 06. 35 0. 6745 -0. 0. 434 0. 861 02. 35 0. 6745 -0. 0. 434 0. 861 02. 35 0. 6745 -0. 0. 434 0. 861 02. 35 0. 6745 -0. 0. 434 0. 861 02. 32 0. 4753 -0.		DRAG	1407 0986 0713 0512 1350	0949 0649 14347 0886	0602 0423 1267 0866 0563	0408 1201 0797 0496 0380	1122 0711 0439 0370 1069	0654 0759 0759 0916 0916
REVN. HRCH. JRCJD. LIFT. 0. 447 0. 902 06. 36 0. 7697 0. 444 0. 892 04. 25 0. 6528 0. 447 0. 902 06. 35 0. 5428 0. 447 0. 902 02. 13 0. 4622 0. 447 0. 903 02. 13 0. 2148 0. 440 0. 860 06. 35 0. 7927 0. 440 0. 861 06. 35 0. 2392 0. 440 0. 861 06. 35 0. 6393 0. 440 0. 861 06. 35 0. 6745 0. 440 0. 861 06. 35 0. 6745 0. 434 0. 861 06. 35 0. 6745 0. 434 0. 861 06. 35 0. 6745 0. 434 0. 861 06. 35 0. 4978 0. 434 0. 879 06. 35 0. 4978 0. 435 0. 801 06. 37 0. 4978 0. 435 0. 801 06. 37 0. 4378 0. 435 0. 801 06. 37 0. 4378 0. 435 0. 70 0. 70 0. 70 0. 436 0. 70 0. 70 0. 4188 0. 434 0. 70 0. 6896 0. 434 0. 70 0. 40 0. 4188 0. 4		-	0. 150 0. 150 0. 153 0. 123 0. 141	ललनल	00000	0. 079 0. 107 0. 101 0. 078	00000	
76. Y. H.C.H. 136. 10. 4447 0. 8948 0.6. 0. 4447 0. 8948 0.6. 0. 4447 0. 8948 0.6. 0. 4447 0. 8948 0.6. 0. 4447 0. 8848 0.6. 0. 4440 0. 8848 0.6. 0. 4448 0. 8848 0.6. 0. 434 0. 8848 0.6. 0. 434 0. 8848 0.6. 0. 434 0. 734 0. 734 0. 6948 0.6. 0. 434 0. 734 0. 734 0. 6948 0.6. 0. 434 0. 734 0. 434 0. 734		-		6739 6744 6739 6745 6745		2261 8019 7153 4753	8117 6896 4399 1973 8071	44444444444444444444444444444444444444
## CCCCC CCCCC CCCCC CCCCC CCCCC CCCCC CCCC		1 KC 1 D.						
\(\text{T} \) \qu		HACH.		C. 882 C. 881 C. 880 C. 860 C. 860	ರರವರ			
		REYR.	4444	44444	****	4444	4444	44444
		4	000 000 000 000		*5000	013 022 022 024 024		

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TABLE 3(F) CLERN HIRCRRFT ETA = +10 ETR(T) = +1/2

SER RE	REVK. MACH.	H. JHCJD.	LIFT.	PITCH.	DRAG	RORMAL	HX I AL.	CLSQ.	BASE.	AINC.	St. 1P.	CR0SS.	YAK M.	ROLL N	RANG.	SIDE F
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	460 454 457 457 457 457 457 457 457 457 457	901 06.33 699 04.24 899 02.40 901 -00.05 879 06.34	0. 7795 0. 6482 0. 4782 0. 2364 0. 7876	-0.1369 -0.1638 -0.2002 -0.1887 -0.1456	0.1484 0.1051 0.0728 0.0542 0.1378	-0. 7912 -0. 6543 -0. 4806 -0. 2364 -0. 2982	-0.0568 -0.0550 -0.0533 -0.0524 -0.0479	0, 6074 0, 4200 0, 2205 0, 0357 0, 6203	0. 0023 0. 0049 0. 0020 0. 0020	06. 24. 24. 06. 06. 04. 24. 06. 04. 04. 04. 04. 04. 04. 04. 04. 04. 04	.00.01 .00.01 .00.01 .00.02	0. 0007 0. 0007 0. 0034 0. 0042 0. 0007	0.0011 0.0011 0.0020 0.0024 0.0015	-0.0010 0.0002 0.0010 0.0007 -0.0010	179.9 180.0 180.0 179.9	-0. 0008 -0. 0008 -0. 0035 -0. 0043 -0. 00043
00000000000000000000000000000000000000	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	660 04.24 679 02.11 680 -00.02 689 06.36 661 04.25	0. 6608 0. 4988 0. 2640 0. 7973 0. 6726	-0.1699 -0.1968 -0.1817 -0.1385	0, 0946 0, 0673 0, 0490 0, 1346 0, 0944	-0, 6661 -0, 5010 -0, 2640 -0, 8074 -0, 6779	-0, 0436 -0, 0471 -0, 0472 -0, 0433 -0, 0423	0, 4365 0, 2486 0, 0696 0, 6355 0, 4523	0. 0018 0. 0018 0. 0019 0. 0020 0. 0019	04, 24 00, 24 06, 02 04, 25	(0.01 (0.01 (0.01 (0.01 (0.01	0.0001 0.0039 0.0046 0.0047 0.0018	0.0011 0.0022 0.0023 0.0018	0.0001 0.0011 0.0008 -0.0004 0.0004	1 1 80 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.0000 -0.0040 -0.0047 -0.0018
014 0. 015 0. 015 0. 017 0.	460 (1.86 463 (1.86 453 (1.83 453 (1.84 453 (1.84	860 02.13 861 -00.01 839 06.34 840 04.26	0. 2642 0. 2642 0. 7977 0. 6948 0. 5257	-0.1884 -0.1673 -0.1422 -0.1658 -0.1767	0, 0623 0, 1263 0, 1264 0, 0888 0, 0599	-0. 5193 -0. 2643 -0. 8069 -0. 6996	-0, 0412 -0, 0434 -0, 0351 -0, 0351 -0, 0355	0, 2673 0, 0697 0, 6362 0, 4826 0, 2762	0.0018 0.0018 0.0021 0.0019 0.0017	02. 13 -00. 01 06. 34 07. 26	-(10, 02 -(10, 02 -(10, 04 -(10, 02	0, 0039 0, 0052 0, 0045 0, 0040 0, 0040	0, 0025 0, 0030 0, 0018 0, 0014 0, 0025	0.0013 0.0010 0.0003 0.0003 0.0012	180.0 180.0 180.0 180.0	-0. 0040 -0. 0053 -0. 0016 -0. 0011
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	453 0.8 470 0.8 470 0.8 467 0.7 470 0.8	8738 00, 00 8700 06, 34 8700 04, 29 798 02, 15 8700 00, 00	0. 2834 0. 8094 0. 7325 0. 2323	-0.4530 -0.4532 -0.4532 -0.4536	0. 0410 0. 1232 0. 0834 0. 0517 0. 0403	-0. 2535 -0. 8581. -0. 7368 -0. 5040	-0.0395 -0.0341 -0.0265 -0.0314 -0.0314	0, 0641 0, 6550 0, 5365 0, 2522 0, 0564	0.0016 0.0019 0.0018 0.0015	00.00 06.34 04.29 02.45 00.00	(10, 02 (10, 02 (10, 02 (10, 02	0.0041 0.0014 0.0046 0.0031 0.0031	0.0025 0.0017 0.0027 0.0020 0.0028	0.0009 0.0017 0.0009 0.0013	4 4 4 4 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9	-0.0042 -0.0015 -0.0047 -0.0032 -0.0051
0.26 0.27 0.27 0.28 0.30 0.30 0.30	4444 4444 99999 99999	750 06.34 750 04.25 751 02.12 750 00.00	0. 8351 0. 7173 0. 4707 0. 2262 0. 8353	-0.1662 -0.1539 -0.1501 -0.1412 -0.1756	0. 1155 0. 0740 0. 0487 0. 0388 0. 1108	-0. 2209 -0. 4723 -0. 2263 -0. 2263	-0. 0212 -0. 0189 -0. 0236 -0. 0373	0, 6973 0, 3145 0, 2214 0, 0511 0, 6976	0.0018 0.0016 0.0016 0.0016	06. 35 04. 25 00. 25 06. 27		0, 0046 0, 0033 0, 0045 0, 0052 0, 0053	0.0025 0.0024 0.0027 0.0027 0.0025	0.0036 0.0015 0.0012 0.0010	180.0 180.0 180.0 180.0	0.0047 0.0034 0.0038 0.0038
031 0, 032 0, 033 0, 036 0,	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	699 04. 24 700 02. 40 699 00. 00 500 06. 20 500 04. 13	0.6745 0.4485 0.2184 0.7754 0.5754	-0. 14462 -0. 1462 -0. 1462 -0. 1486 -0. 1486	0.0674 0.0472 0.0392 0.0955	-0.6777 -0.4501 -0.2185 -0.7810 -0.5968	-0, 0360 -0, 0377 -0, 0377 -0, 0092 -0, 0460	0, 4348 0, 2011 0, 0476 0, 5007 0, 3525	0.0017 0.0016 0.0016 0.0020 0.0020	04. 20 00. 00 04. 20 04. 20	-(10.01 -(10.01 -(10.01	0.0047 0.0037 0.0031 0.0018	0,0025 0,0027 0,0028 0,0027 0,0027	0.0022 0.0012 0.0008 0.0017 0.0021	1 1 80.00 0 1 1 1 80.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0048 0.0038 0.0038 0.0038
038 0. 039 0.	447 G. 49 449 G. 5G	99 02.07 01 00.00	0. 4012 0. 1993	-0.1350 -0.1237	0, 0436	-0, 4026 -0, 1994	-0.0275 -0.0346	0, 1609 0, 0396	0. 0016 0. 0017	00.00	-(10.01	0.0044	0. 0024 0. 0025	0.0014 0.0011	180.0 - 180.0 -	0. 0048 0. 0049

TABLE 4 CLERN A)RCRAFT TAJLPLANE OFF

	RANG. SIDE F		-090. 0 -0.0099 -090. 0 -0.0049 -090. 0 -0.0001 -090. 0 -0.0201 -090. 0 -0.0095	-090. 0 -0. 0048 -090. 0 -0. 0001
	ROLL M RA	0. 0013 -09 0. 0007 -09 0. 0004 -09 0. 0002 -09 0. 0006 -09	0. 0004 -09(0. 0003 -09(0. 0003 -09(0. 0008 -09(0. 0005 -09(0. 0004 - 090 0. 0003090
	YAN M.	-0, 0039 -0, 0039 -0, 0021 -0, 0001	-0, 0037 -0, 0019 -0, 0001 -0, 0068 -0, 0035	-0.0018 -0.0001
	CR055.	0. 00274 0. 0066 0. 0043 0. 0003 0. 0160	0, 00085 0, 00042 0, 0000 0, 0427 0, 0083	
	St. 1P.	(14, 05 (8), 02 (11, 04, 04) (10, 00)	02. 02 01. 01 00. 00 04 03 02. 01	(11, 96 (16, 96
	ATRC.	00, 05 00, 05 00, 05 00, 08	00, 08 00, 08 00, 08 00, 04 00, 04	00. 04 00. 04
L	BASE	0.0013 0.0017 0.0015 0.0018 0.0018	0. 0045 0. 0045 0. 0043 0. 0044 0. 0044	0. 0016 0. 0014
INTELLIBRATE OFF	CL SQ.	C. 0492 C. 0447 C. 0463 C. 0463 C. 0464	C. 0446 C. 0450 C. 0443 C. 0273 C. 0273	0, 0270 0, 0275
-	RXIM.	2220 -0,0447 2117 -0,0452 2150 -0,0454 2073 -0,0456 2112 -0,0335	2116 -0,0326 2126 -0,0326 2110 -0,0326 1655 -0,029	-0, 0289 -0, 0293
	KORHAL	-0,2220 -0,2417 -0,2450 -0,2073	-0,2416 -0,2426 -0,2410 -0,4655 -0,1655	1648 1650
	DRAG	0, 0475 0, 0474 0, 0469 0, 0475 0, 0363	0.0346 -0.5 0.0345 -0.5 0.0341 -0.6 0.0327 -0.4	0. 0306 -0. 0. 0308 -0.
	P11CH.	-0.0816 -0.0815 -0.0817 -0.0818 -0.0383	-0.0384 -0.0384 -0.0381 -0.0281 -0.0273	-0. 0270 -0. 0269
	DREAD, LIFT,	0.2218 0.2115 0.2148 0.2071 0.2111	0. 2125 0. 2125 0. 2109 0. 1654 0. 1653	0.1647 -0.0270 0.1648 -0.0269
	DREAD.	20 20 20 20 20 20 20 20 20 20 20 20 20 2	00. 08 00. 08 00. 08 00. 04	00. 00. 04 04.
	RACH.	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0. 803 0. 803 0. 796 0. 504 0. 500	
	SER REYR.	076 0, 457 0, 900 077 0, 457 0, 904 078 0, 457 0, 900 079 0, 460 0, 902 082 0, 462 0, 800	083 0, 458 (r. 800 084 0. 460 0. 803 085 0. 458 0. 798 088 0. 444 0. 501 009 0 444 0. 500	090 (), 444 (), 499 091 (), 444 (), 499

TABLE 4 CLEBN AJRCRAFT TAJLPLANE OFF

	RANG. SIDE F	179. 9 0. 0035 179. 9 0. 0035 179. 9 0. 0029 180. 0 0. 0024 180. 0 0. 0010	180. 0 0. 0007 180. 0 -0. 0012 180. 0 -0. 0021 180. 0 0. 0036 180. 0 0. 0027	180. 0 0.0025 180. 0 0.0029 180. 0 0.0009 180. 0 0.0005 180. 0 -0.0005	180.0 -0.0013 180.0 0.0016 180.0 0.0016 180.0 0.0013 180.0 0.0008	180. 0 -0. 0002 180. 0 -0. 0002 180. 0 -0. 0006 180. 0 -0. 0009
	ROLL M R	-0.0008 -0.0022 -0.0006 0.0004	0, 0014 0, 0016 0, 0019 0, 0018 0, 0029	0.0004 0.0012 0.0021 0.0017 0.0016	0.0019 0.0030 0.0024 0.0024 0.0028	0.0026 0.0018 0.0019 0.0020
	YAN H.	-0.0004 -0.0006 -0.0007 -0.0003	0.0001 0.0006 0.0000 -0.0013 -0.0007	-0.0002 -0.0002 0.0002 0.0005 0.0005	0.0002 0.0005 0.0006 0.0006	0.0007 0.0002 0.0002 -0.0004
	CROSS.	-0.0036 -0.0036 -0.0030 -0.0023 -0.0041	-0. 0008 0. 0011 0. 0020 -0. 0037 -0. 0028	-0, 0026 -0, 0030 -0, 0010 -0, 0006 0, 0001	0.0012 -0.0017 -0.0017 -0.0016 -0.0009	0. 00001 0. 00003 0. 00005 0. 00005
	St.1P.	100.00 100.00 100.00 100.00	100.00 100.00 100.00 100.00 100.00	- (10, 01 - (10, 01 - (10, 01 - (10, 01 - (10, 01	- (10 . 01 - (10 . 01 - (10 . 01 - (10 . 01 - (10 . 01	
	RINC.	07. 48 06. 40 05. 35 04. 30 03. 28	04. 44 -03. 48 07. 44 06. 42	05, 44 04, 37 03, 32 04, 46 -04, 00	03, 16 07, 29 06, 27 05, 24 04, 20	03. 16 04. 08 -01. 00 -03. 08
	BRSE.	0.0017 0.0018 0.0018 0.0018 0.0019	0, 0017 0, 0017 0, 0016 0, 0013 0, 0013	0, 0015 0, 0016 0, 0018 0, 0014 0, 0015	0.0014 0.0021 0.0017 0.0018 0.0018	0.0015 0.0015 0.0016 0.0016
ELFEMENT OF	CLSQ.	0, 7216 0, 6046 0, 4992 0, 3980 0, 2939	0, 1073 0, 0040 0, 0517 0, 6384 0, 5943	(i, 5609 (i, 4689 (i) 3432 (i) 1099 (i) 0060	0, 0300 0, 5610 0, 3042 0, 3901 0, 2672	0, 4987 0, 0670 0, 0041 0, 0153
=	AXIAL.	-0.0509 -0.0472 -0.0448 -0.0448	-0, 0454 -0, 0430 -0, 0372 -0, 0303	-0, 0243 -0, 0497 -0, 0226 -0, 0226 -0, 0322	-0, 0238 -0, 0444 -0, 0064 -0, 0445	-0.0169 -0.0269 -0.0293 -0.0237
	HORMAL	-0.8638 -0.7881 -0.7443 -0.5460 -	-0.3289 -0.0633 -0.2302 -0.8405 -0.06732 -0.00792 -0.0070	-0, 7546 -0, 6886 -0, 5884 -0, 3324 -0, 0774 -	0.1751 - -0.7703 - -0.7154 - -0.6282 - -0.5386 -	-0.4478 -0.2598 -0.0646 -0.1257 -
	DRAG	0. 1641 0. 1367 0. 1131 0. 0944 0. 0777	0.0534 0.0435 0.0514 0.1363 0.1156	0.0939 0.0737 0.0584 0.0377 0.0322	0.0348 0.1107 0.0861 0.0654	0.0434 0.0332 0.0297 0.0319
	PITCH.	-0.0759 -0.0761 -0.0770 -0.0824 -0.0831	-0.0858 -0.0673 -0.0385 -0.0300	-0.0267 -0.0236 -0.0233 -0.0333 -0.0440	-0. 0568 -0. 0066 0. 0039 0. 0035	-0.0104 -0.0225 -0.0333 -0.0430
	LIFT.	0.8496 0.7776 0.7067 0.6310 0.5423	0.3278 0.0640 -0.2278 0.7991 0.7710	0.7490 0.6848 0.3859 0.3316	-0.1736 0.7623 0.7101 0.6247 0.5361	0. 2591 0. 2591 0. 0650 -0. 1243
	INCID	07. 45 06. 40 05. 35 04. 30	04. 44 -04. 03 -03. 48 -07. 44 06. 42	05. 41 04. 37 03. 32 04. 46	-03. 16 7. 05. 29 05. 24 04. 20	03. 16 01. 08 -01. 00 -03. 06
	ITACH.	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	0. 900 0. 901 0. 899 0. 801	p. 799 p. 799 p. 801 p. 800 p. 800	0 801 0.303 0.300 0.300 0.300	C. 500 C. 501 C. 501 C. 499
	REYN.		4 4 4 4 4 4 4 4 4 4 4 8 8 8 8	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 C C C C C C C C C C C C C C C C C C C
	SER	003 003 004 005	007 008 008 012 013	2 2 2 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	022 022 022 022

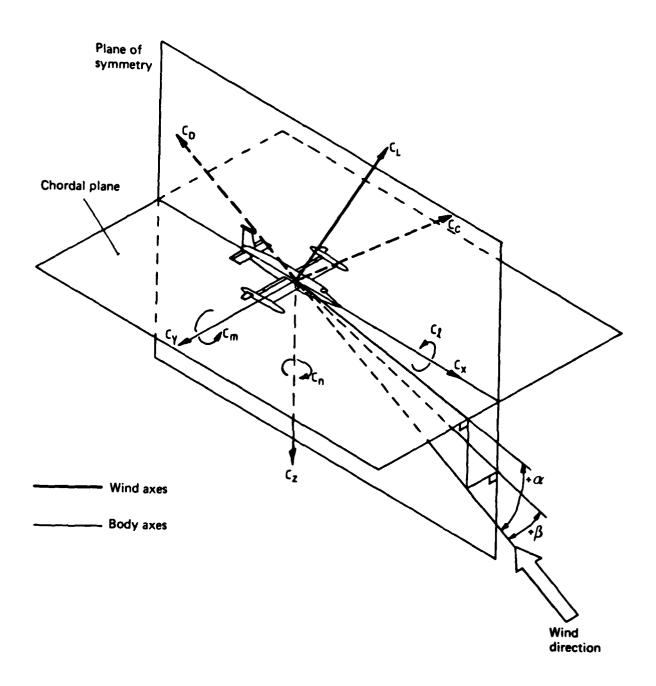


FIG. 1 FORCE AND MOMENT AXES SYSTEM

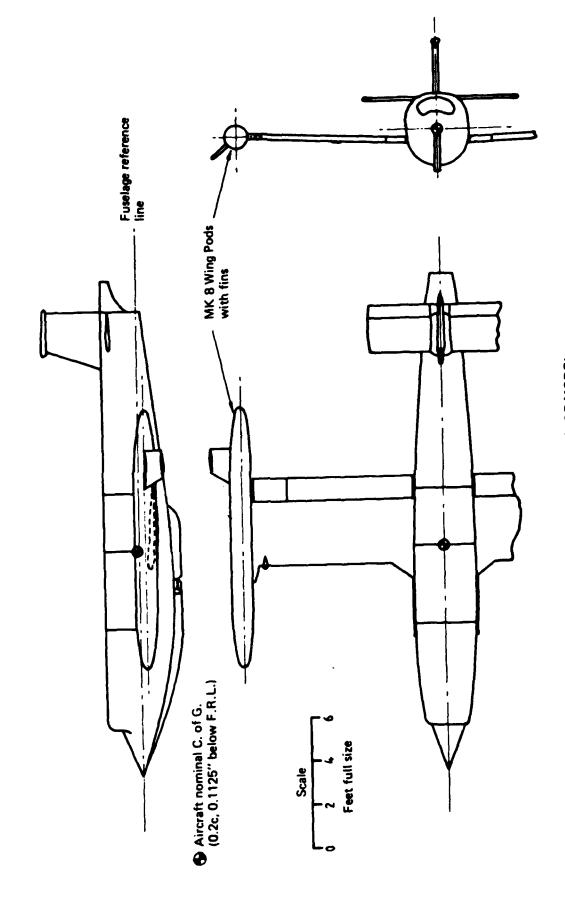


FIG. 2 SKETCH OF MODEL



FIG. 3 PHOTOGRAPH OF MODEL

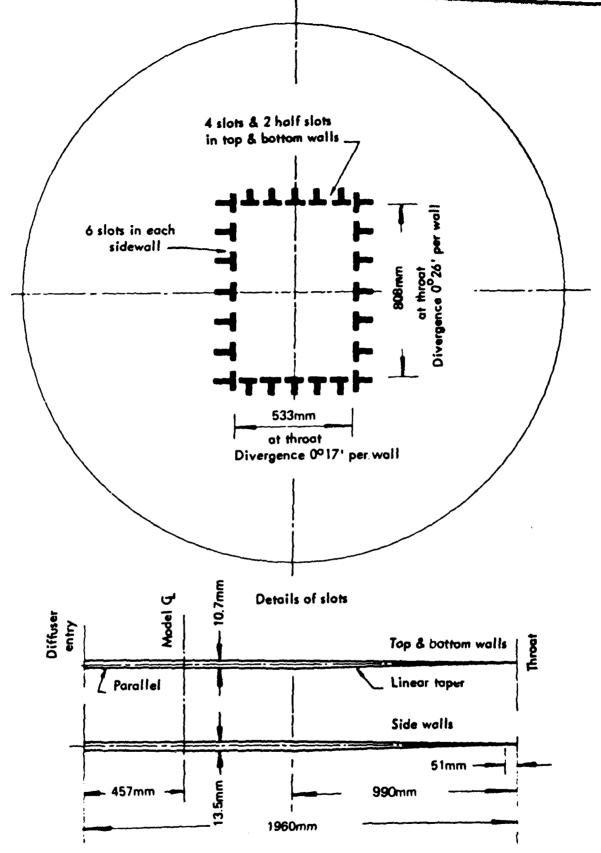


FIG. 4 DETAILS OF SLOTTED TEST SECTION

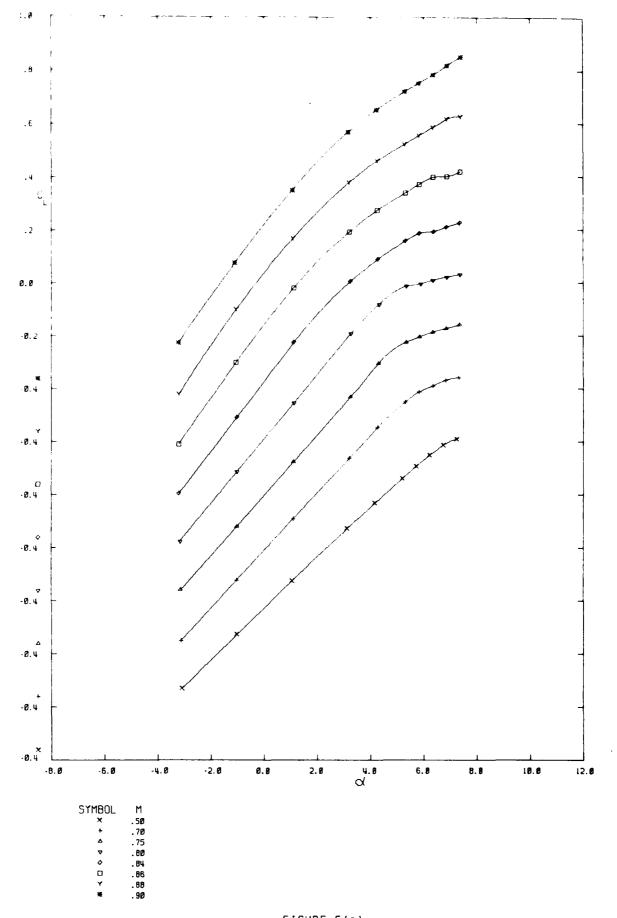


FIGURE 5(a) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE $\eta_{\tau}^{= 3.5}$ η = 0

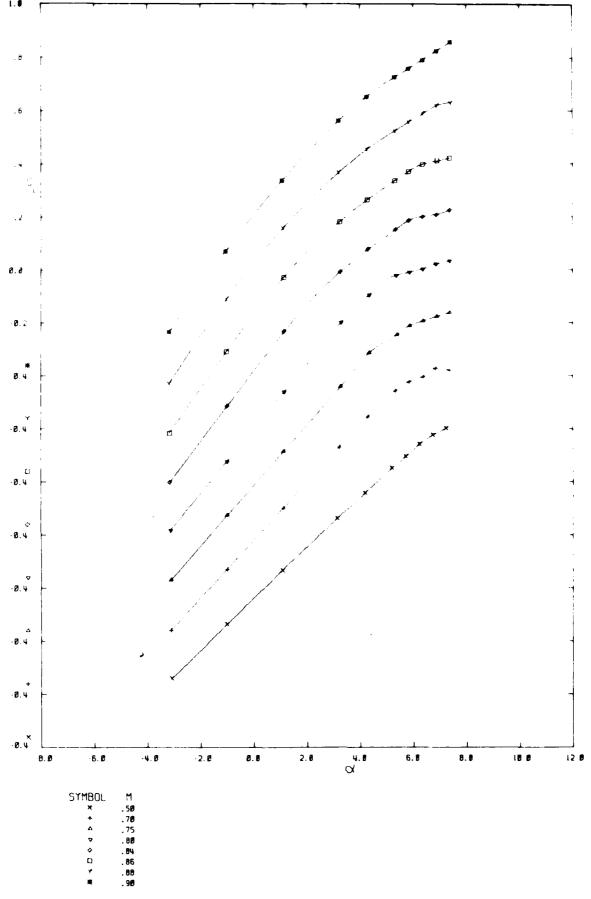


FIGURE 5(b) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE $\eta_{\tau} = 2.5 - \eta = 0$

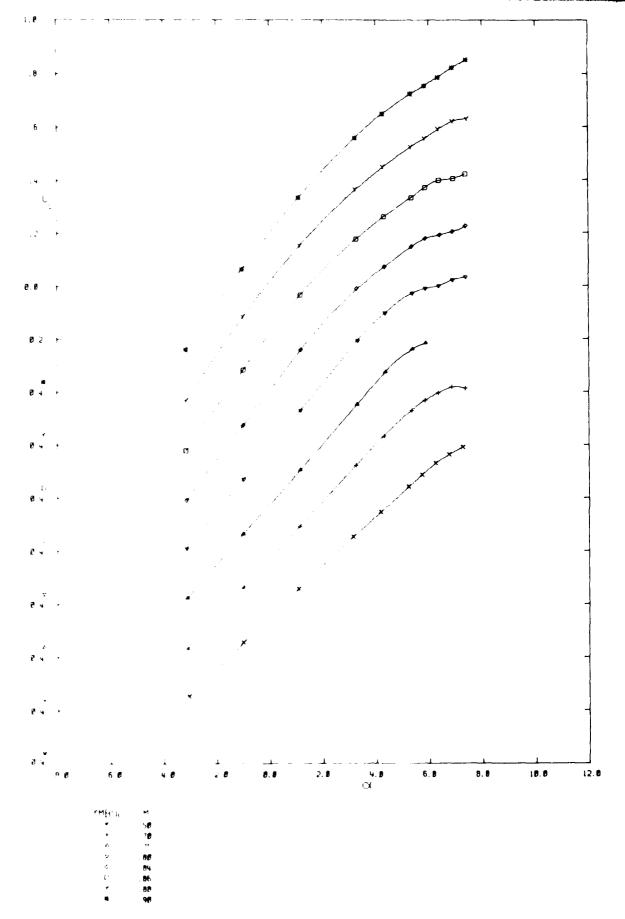


FIGURE 5:01 VHRIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 1.5 - \eta = \emptyset$

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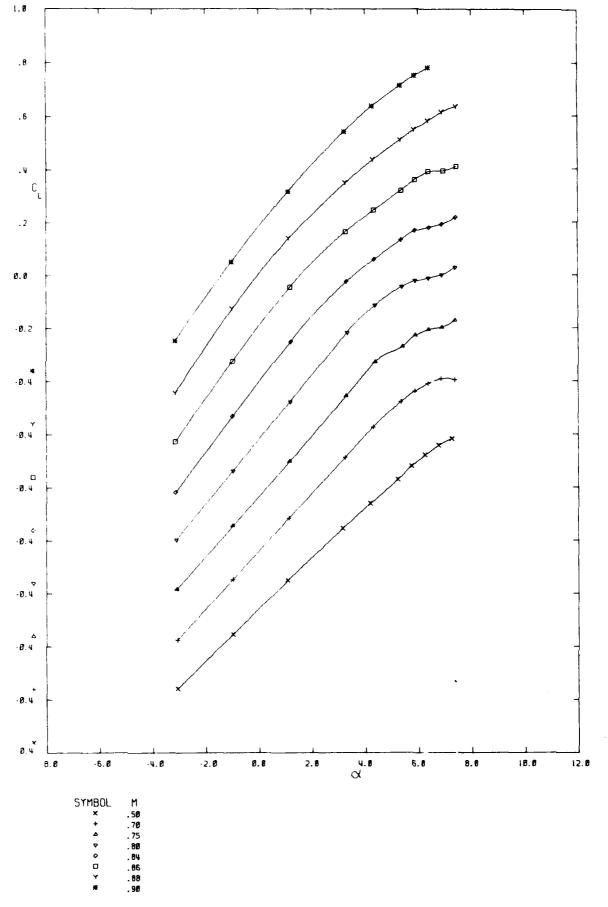


FIGURE 5(d) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 \quad \eta = 0$

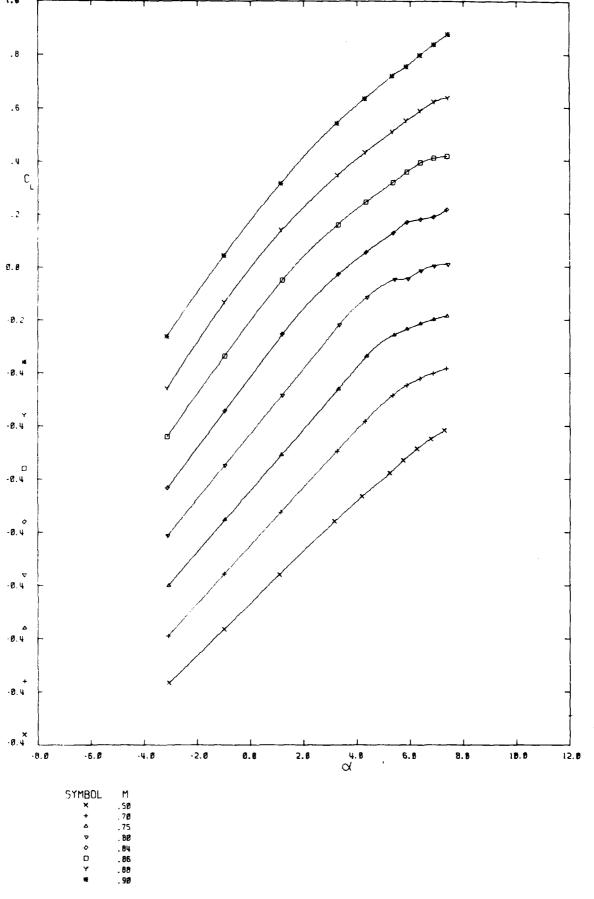


FIGURE 5(e) VARIATION OF L. T COEFFICIENT WITH INCIDENCE. $\eta_{\tau^{\pm}} = 0.5 - \eta_{-} = 0$

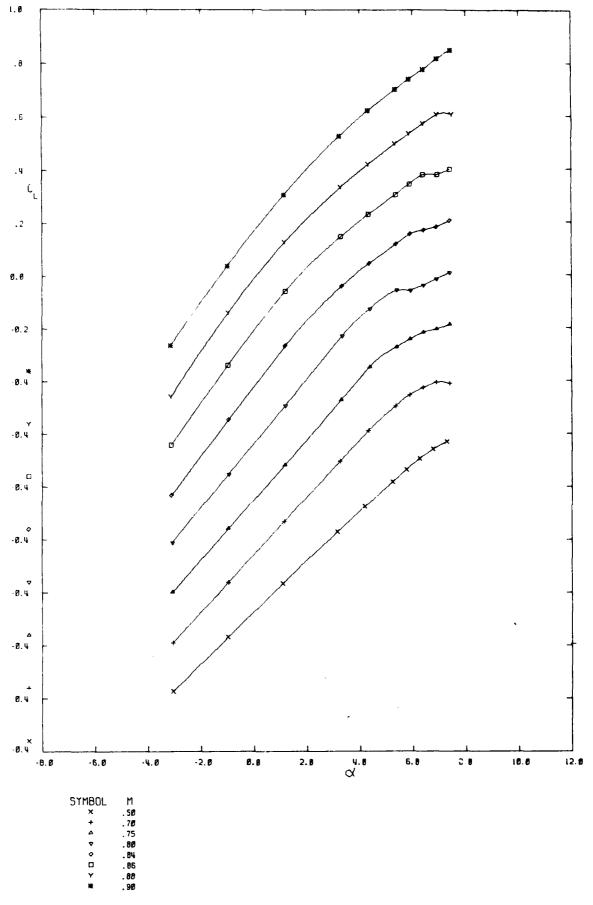


FIGURE 5(f) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = -1.5 \quad \eta = \emptyset$

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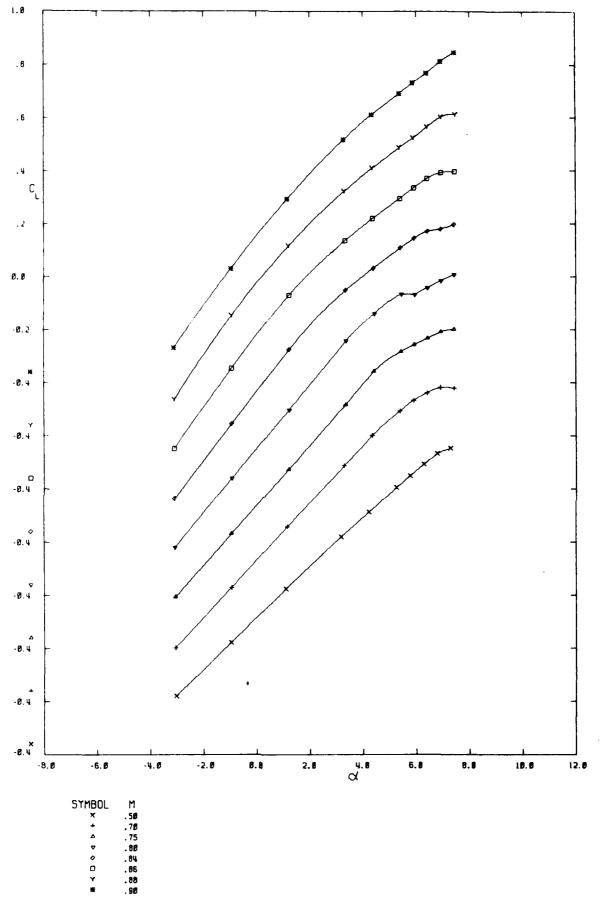


FIGURE 5(e) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = -2.5 \quad \eta = \emptyset$

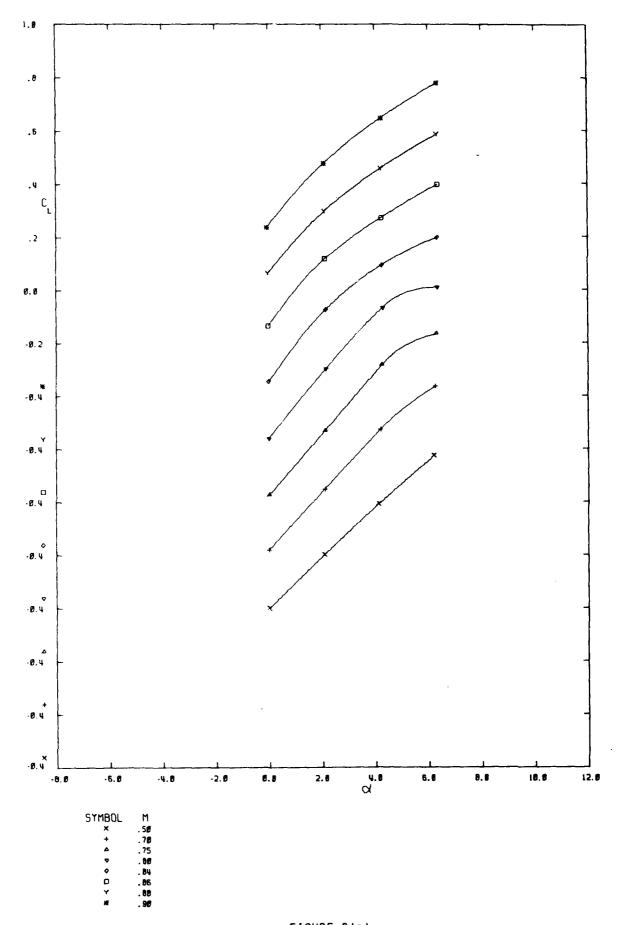


FIGURE 6(a) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 \quad \eta = 10$

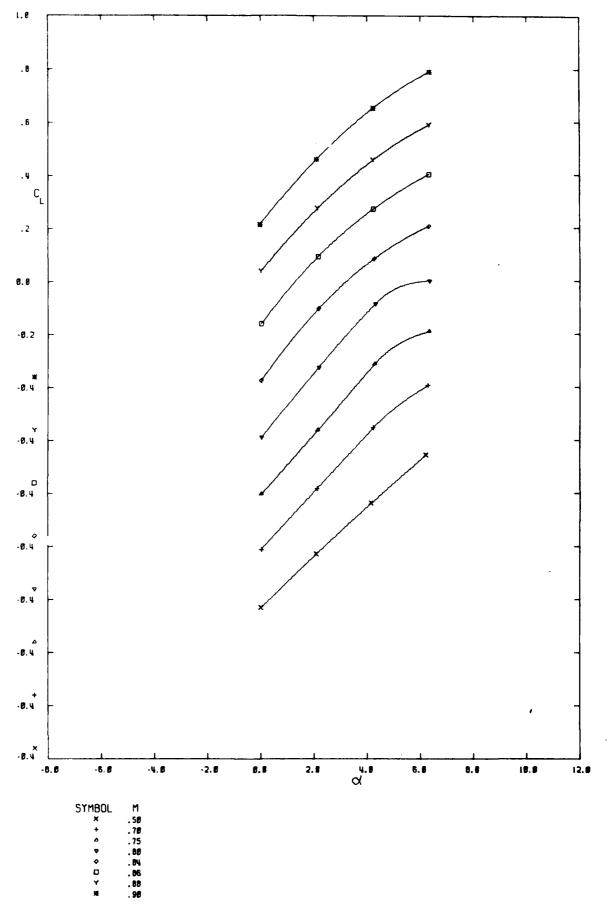


FIGURE 6(b) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. η_{τ} = 0.5 η = 5

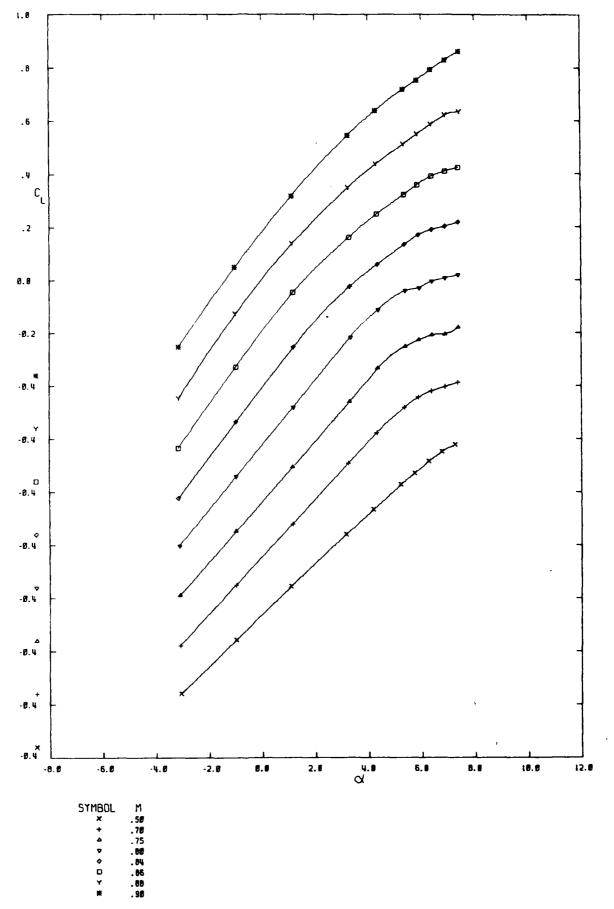


FIGURE 6(c) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_\tau = 0.5 \quad \eta = 0$

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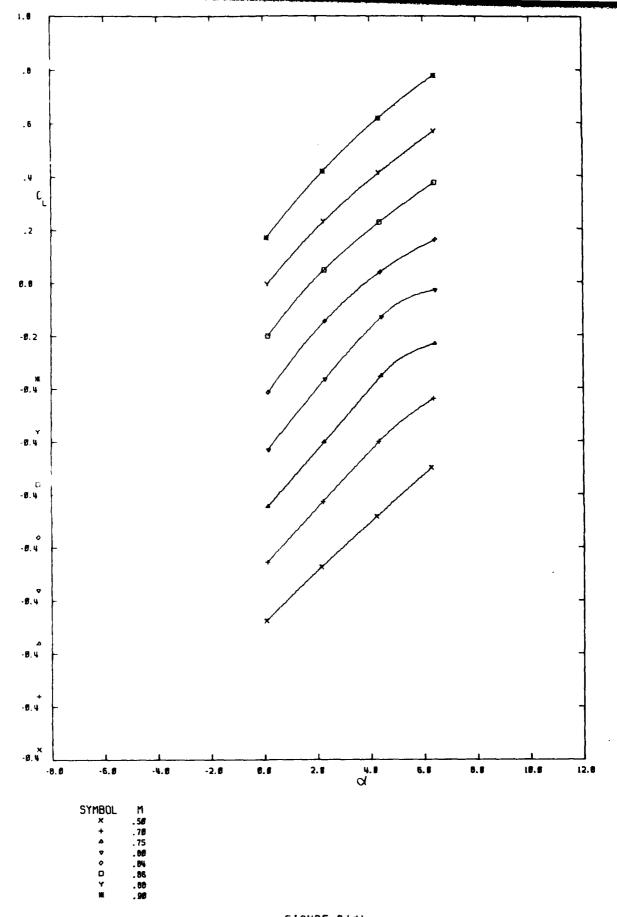


FIGURE 6(d) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 \quad \eta_{-} = -5$

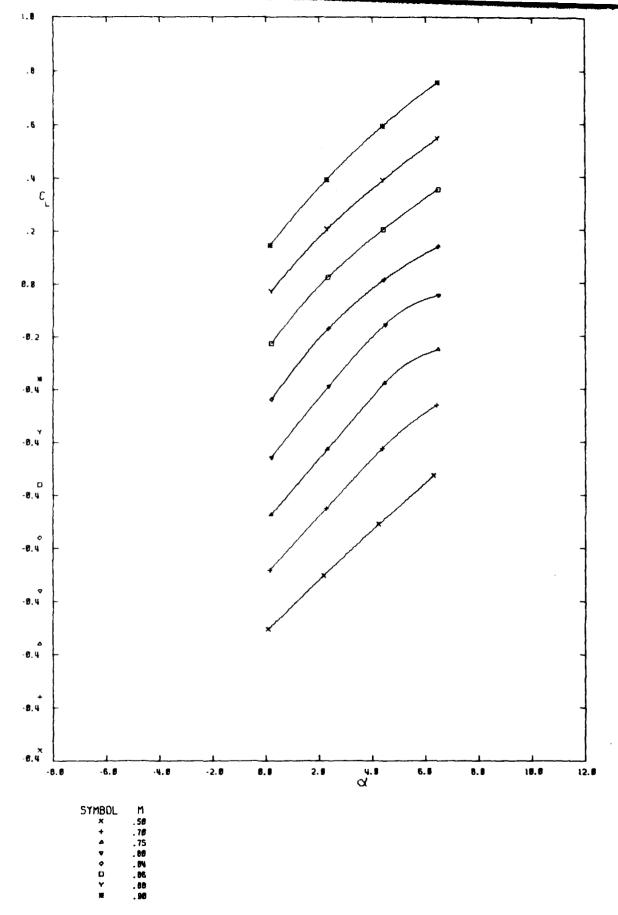


FIGURE 6(*) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. $\eta_{\tau^{\pm}} = 0.5 \quad \eta_{-} = -10$

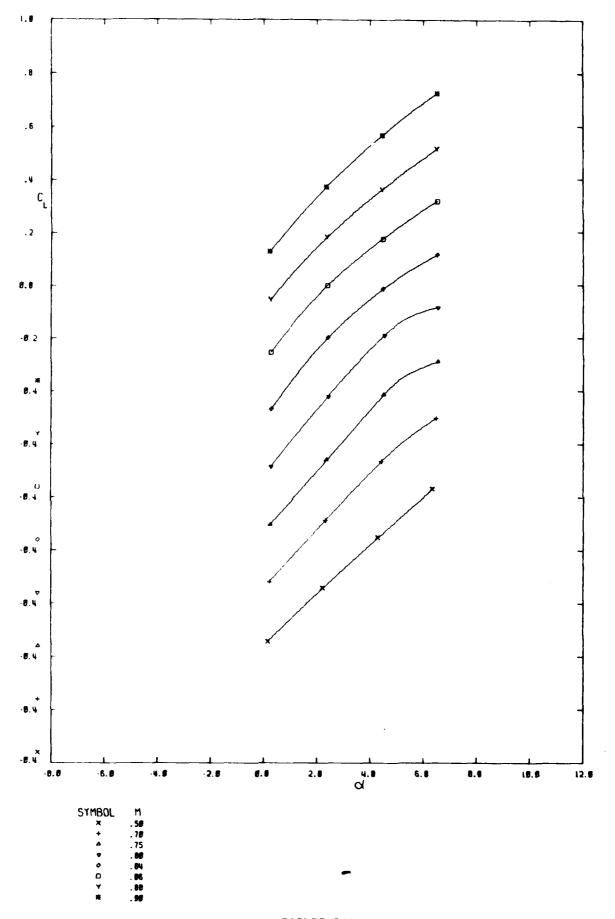


FIGURE 6(f) VARIATION OF LIFT COEFFICIENT WITH INCIDENCE. η_{τ} = 0.5 η_{-} = -15

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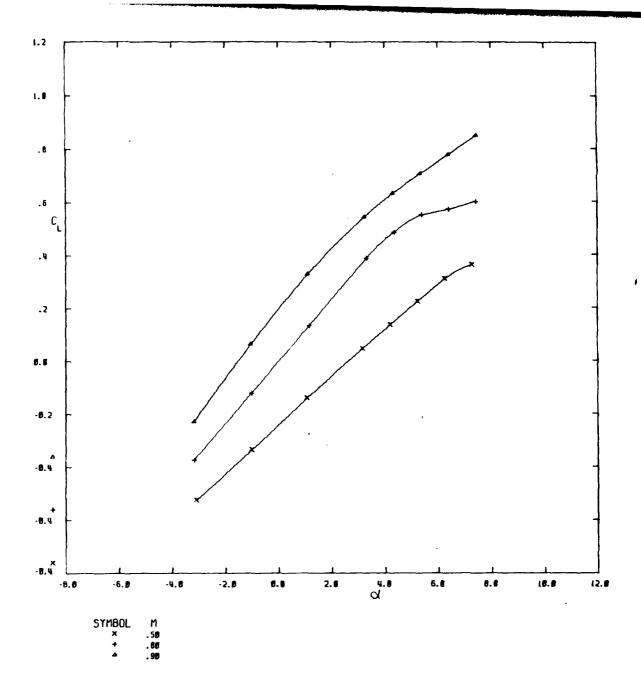


FIGURE 7
VARIATION OF LIFT COEFFICIENT WITH INCIDENCE.
TAIL PLANE OFF.

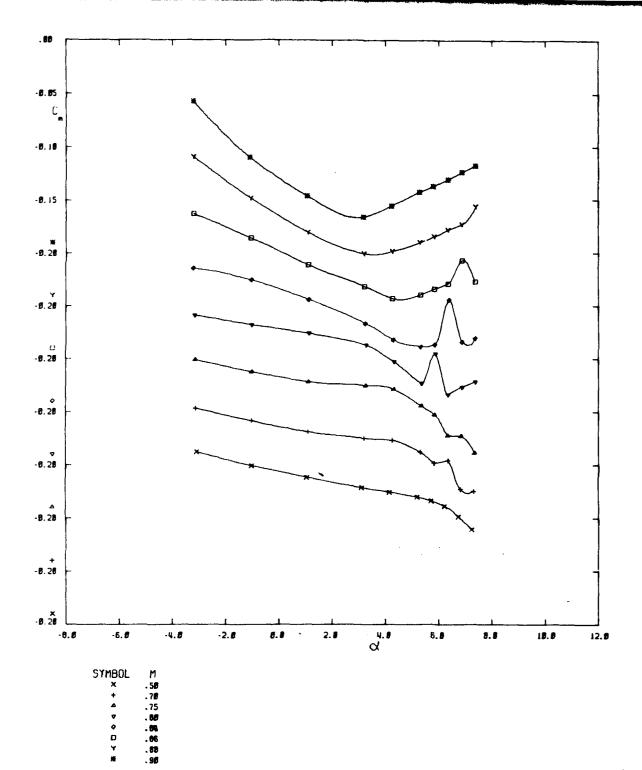


FIGURE 8(%) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 3.5 \quad \eta = 0$

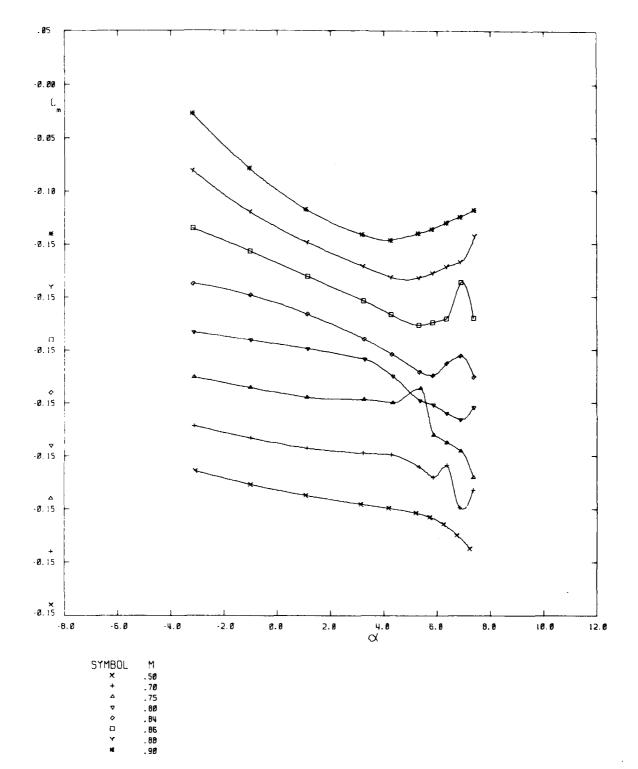
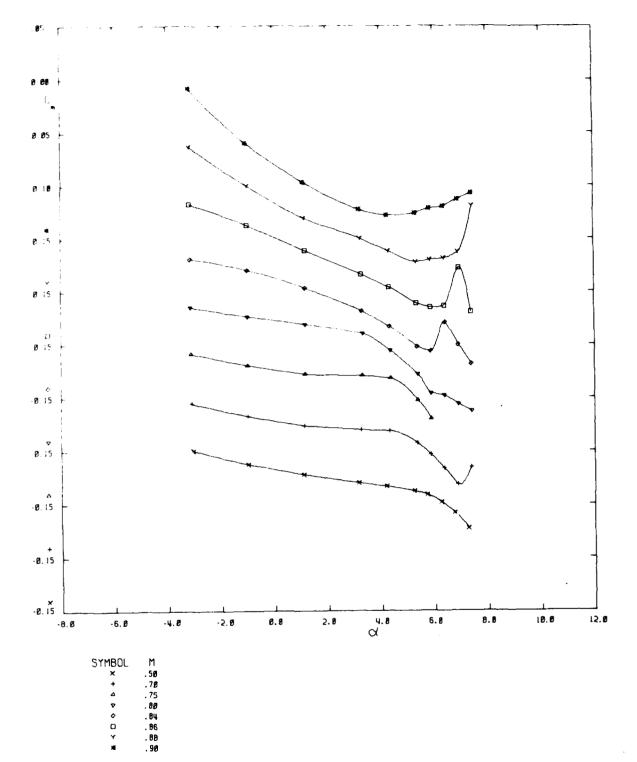


FIGURE 8(b) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 2.5 \quad \eta = 0$

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variation of pitching moment coefficient with incidence. $\eta_{\tau} = 1.5 - \eta = 0$

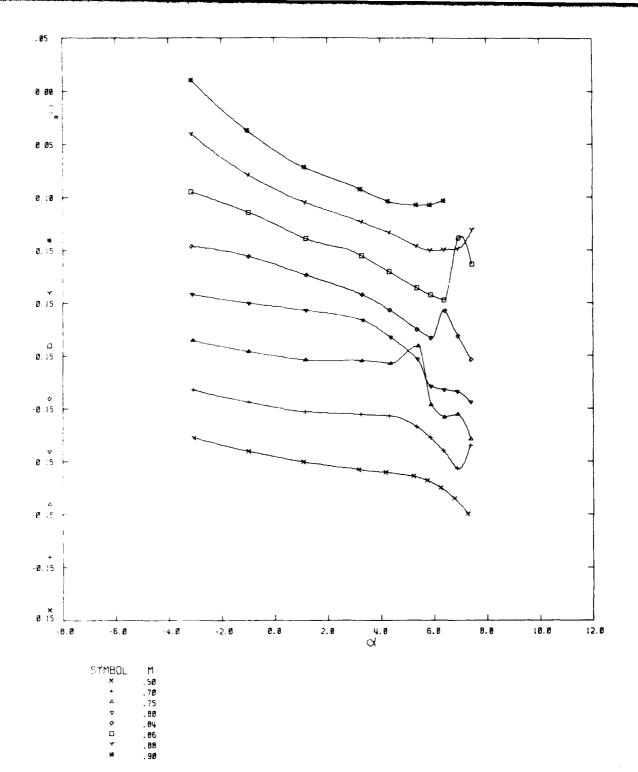
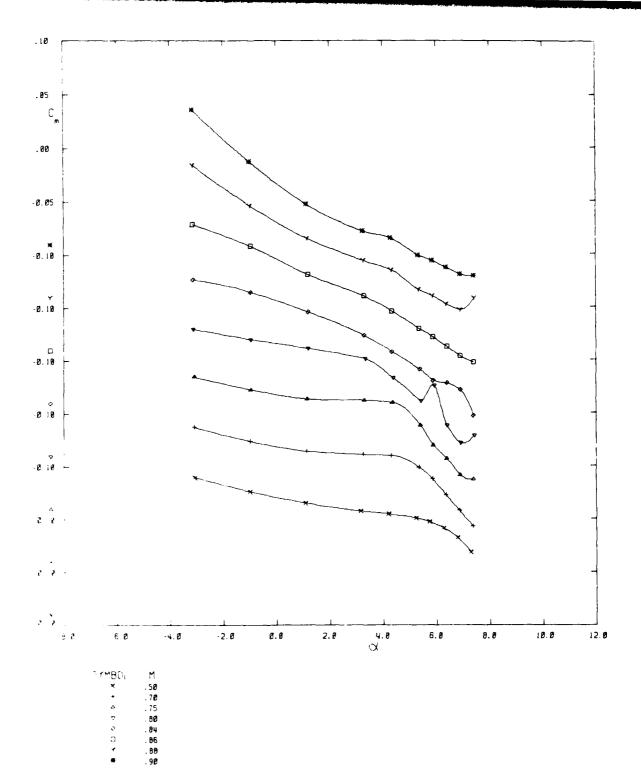


FIGURE 8(d) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 - \eta_{-} = 0$

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FICURE 8(e) variation of pitching moment coefficient with incidence. $\eta_{\tau} = -0.5 - \eta = 0$

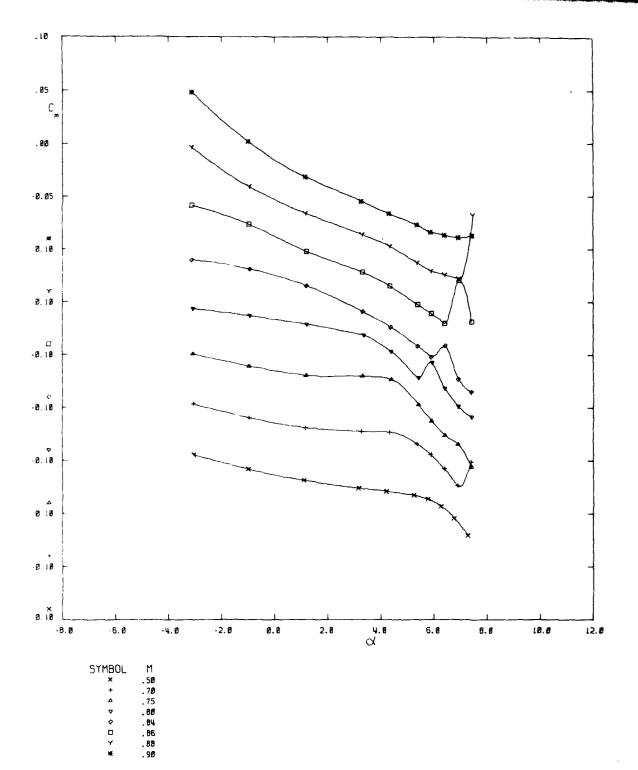


FIGURE 8(f) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = -1.5 \quad \eta = 0$

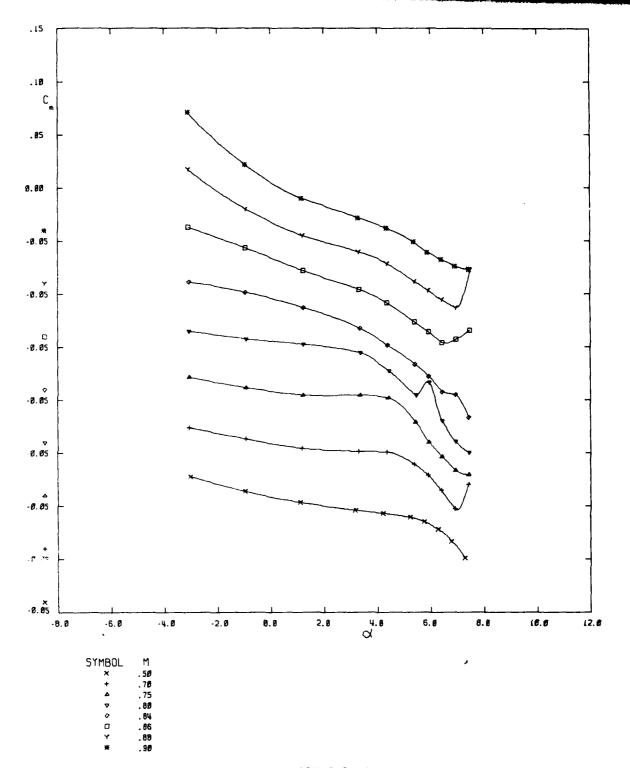
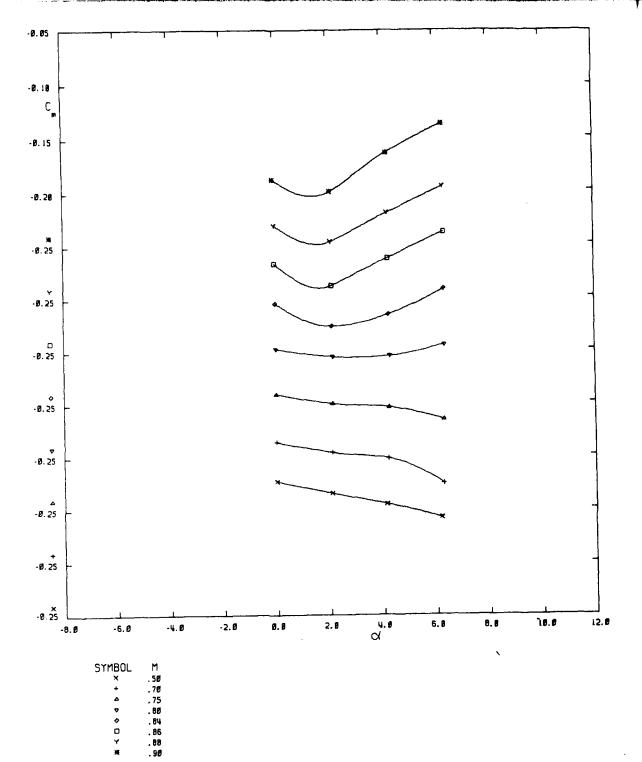


FIGURE 8(0) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_\tau^{=\,-2.5} \quad \eta \approx 0$

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FICURE 9(a) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 \quad \eta = 10$

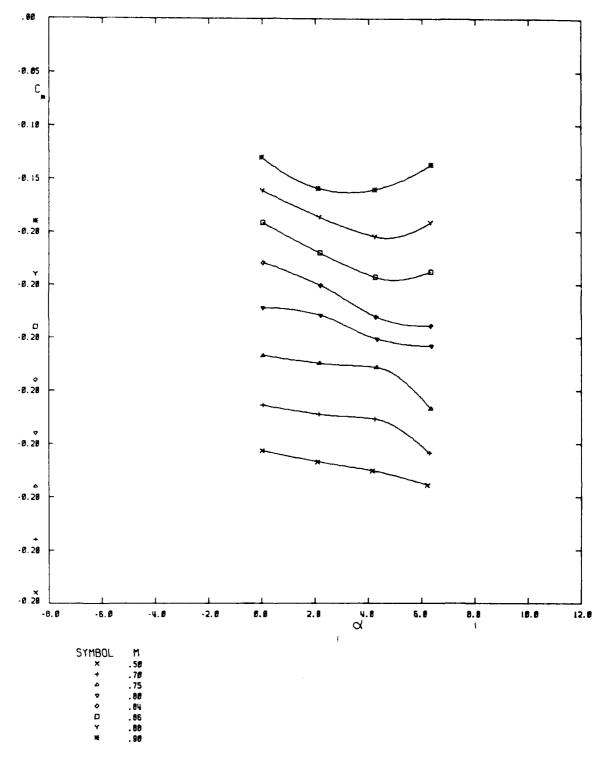


FIGURE 9(b) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\tau} = 0.5 \quad \eta = 5$

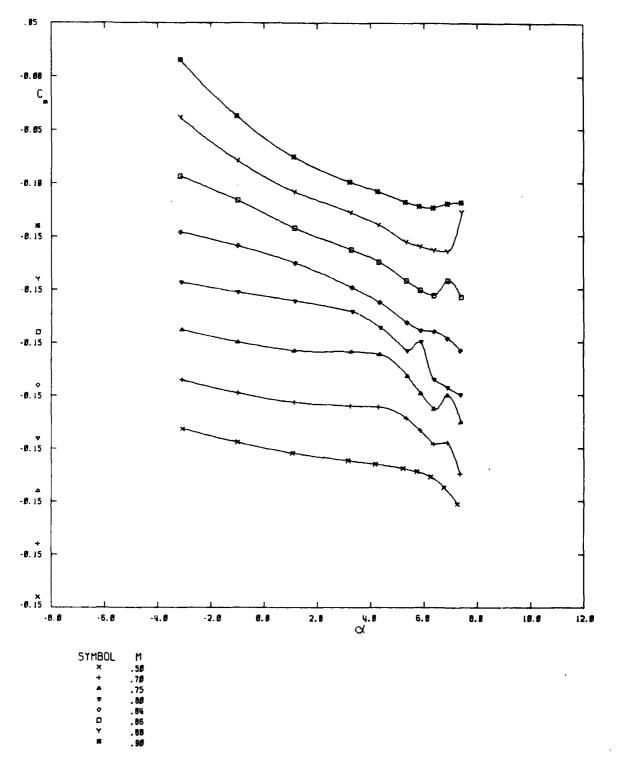
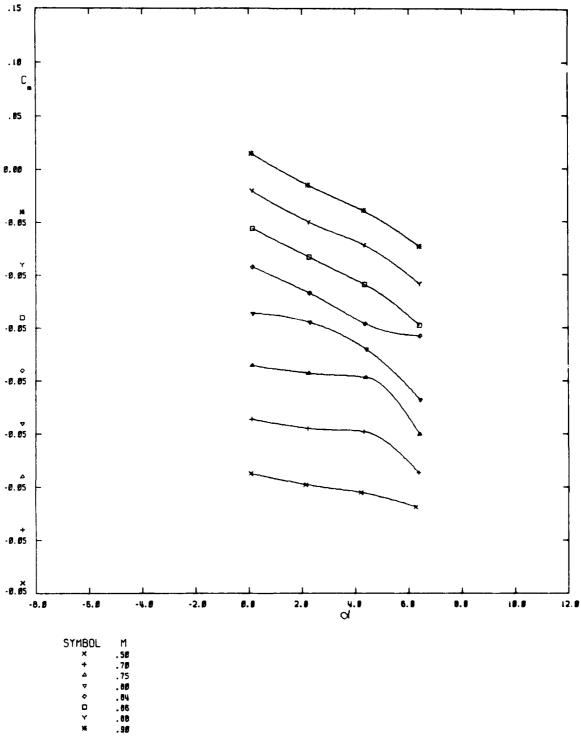


FIGURE 9(c) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. η_{τ} = 0.5 η = 0

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FICURE 9(d)

VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_{\pi^\pm} = 0.5 - \eta_{-\pm} - 5$

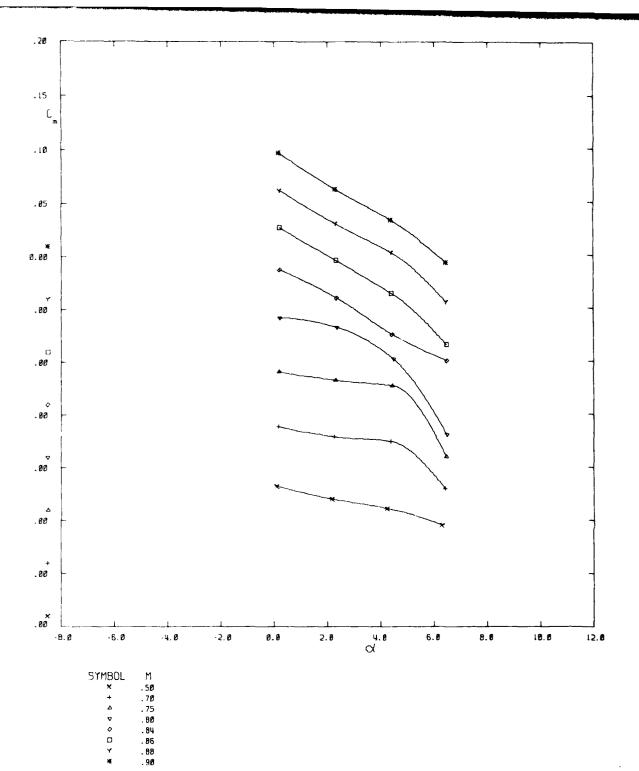


FIGURE 9(e) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. $\eta_\tau = 0.5 \quad \eta = -10$

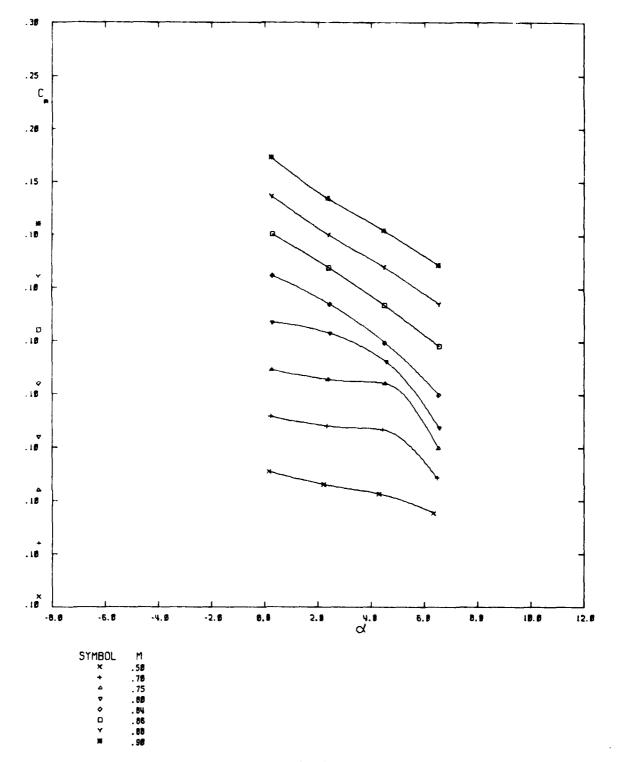


FIGURE 9(1) VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. η_{τ} = 0.5 η = -15

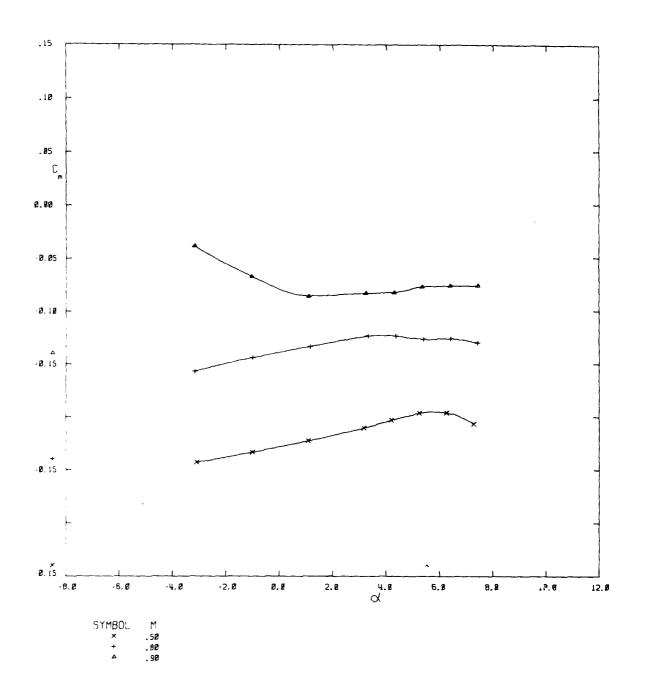


FIGURE 10 VARIATION OF PITCHING MOMENT COEFFICIENT WITH INCIDENCE. TAIL PLANE OFF.

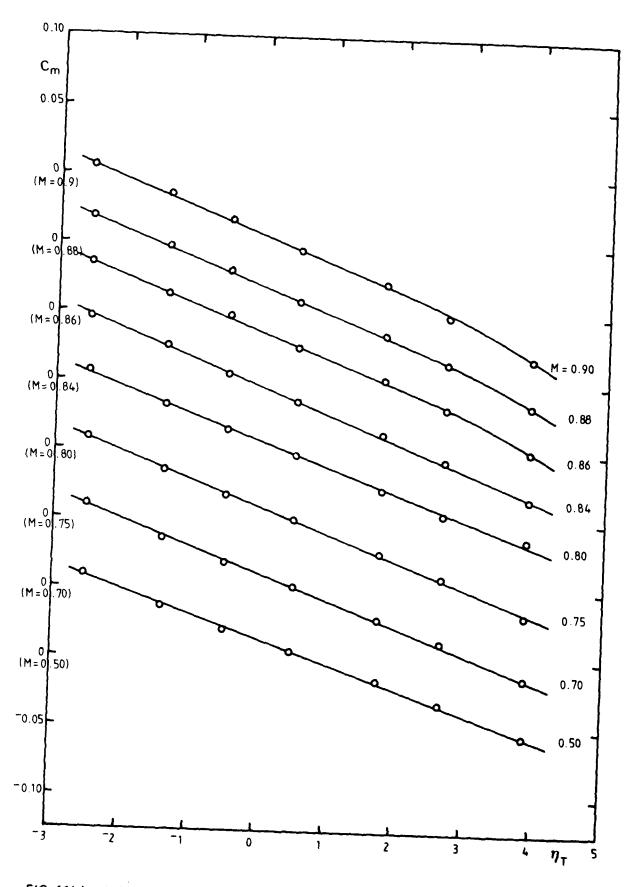


FIG. 11(a) VARIATION OF PITCHING MOMENT COEFFICIENT WITH TAILPLANE ANGLE $(r=0^o;\,\eta=0^o)$

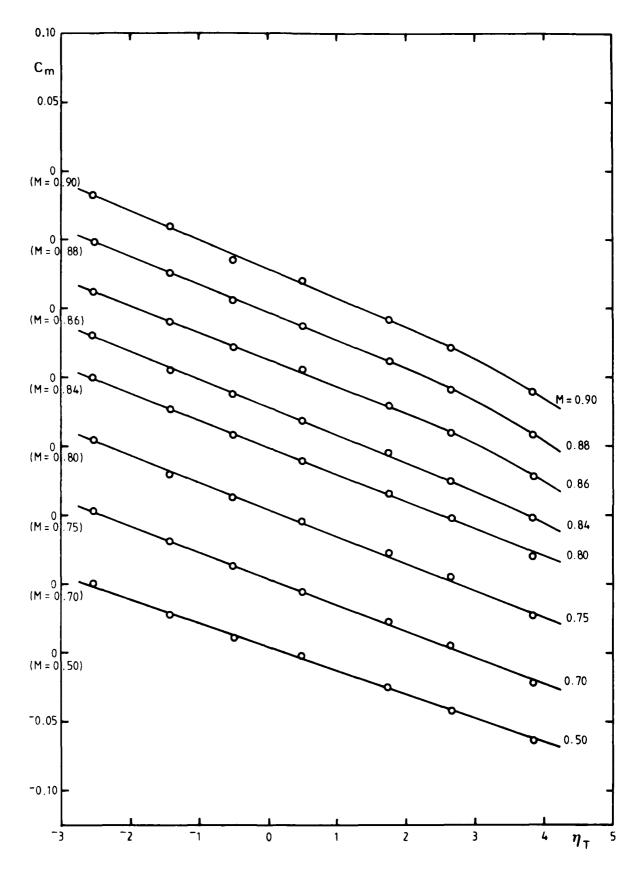


FIG. 11(b) VARIATION OF PITCHING WITH TAILPLANE ANGLE lpha = 2°; η = 0°

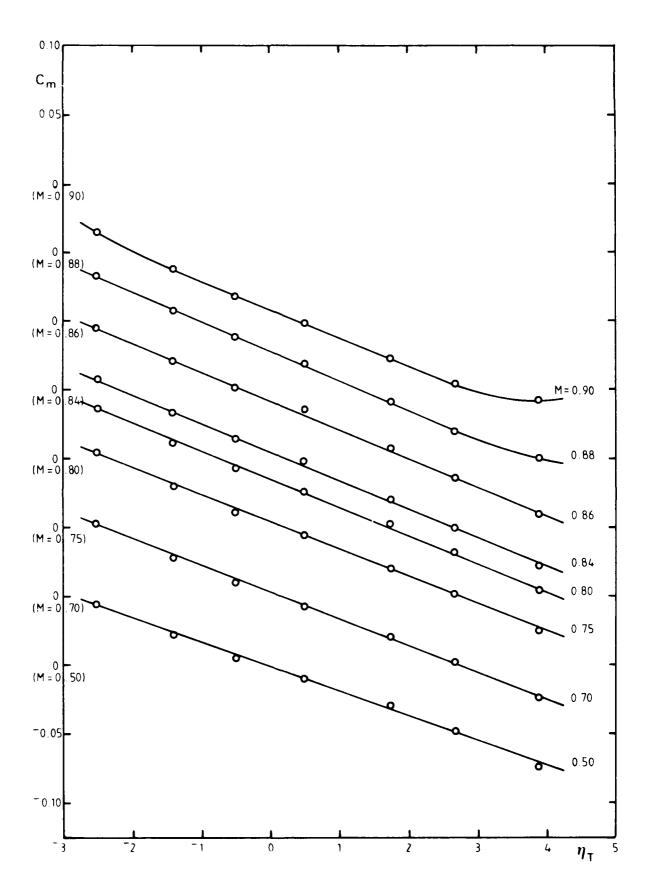


FIG. 11(c) VARIATION OF PITCHING MOMENT COEFFICIENT WITH TAILPLANE ANGLE $_{(Y}$ = 4° ; η = 0°

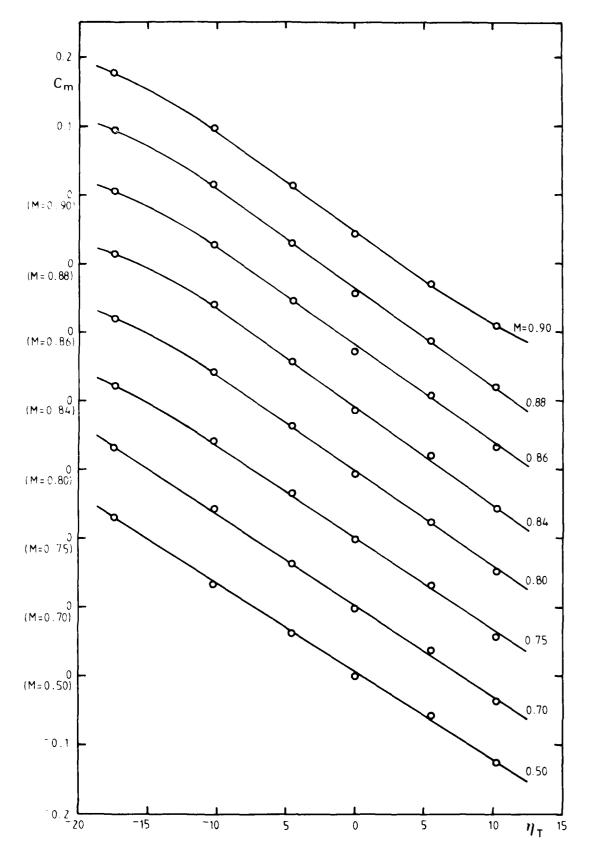


FIG. 12(a) VARIATION OF PITCHING MOMENT COEFFICIENT WITH ELEVATOR ANGLE $\alpha = 0^{\circ}$; $\eta_{\rm T} = \%^{\circ}$

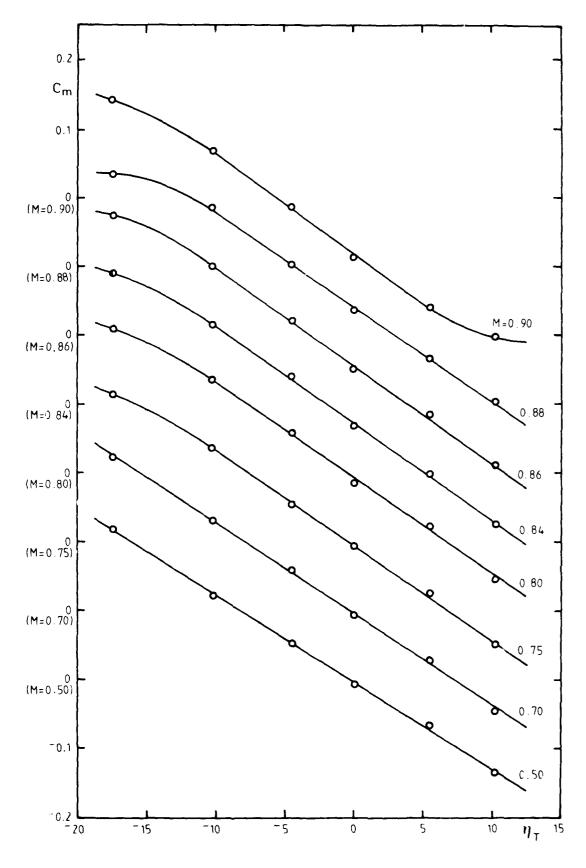


FIG. 12(b) VARIATION OF PITCHING MOMENT COEFFICIENT WITH ELEVATOR ANGLE ' $\alpha = 2^{\circ}$; $\eta_{T} = \%^{\circ}$

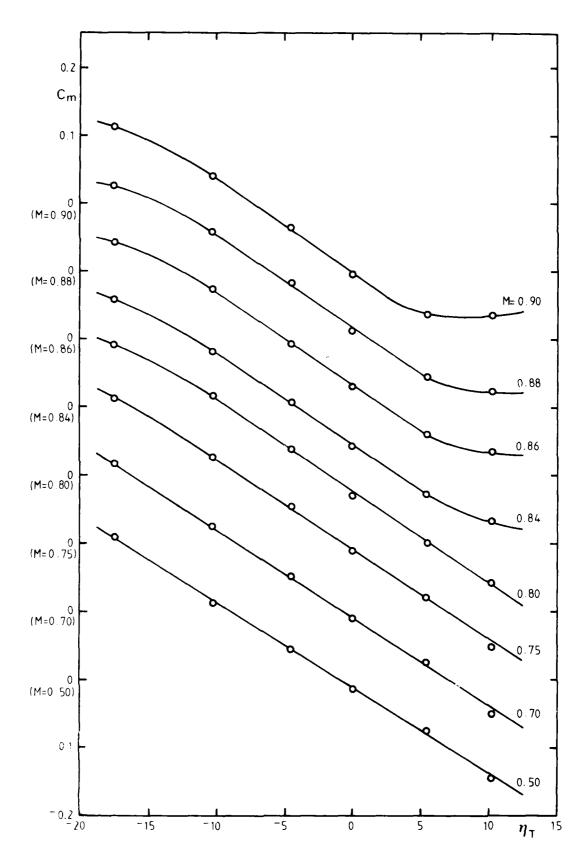


FIG. 12(c) VARIATION OF PITCHING MOMENT COEFFICIENT WITH ELEVATOR ANGLE $\alpha = 0^{0}$; $\eta_{T} = \%^{0}$

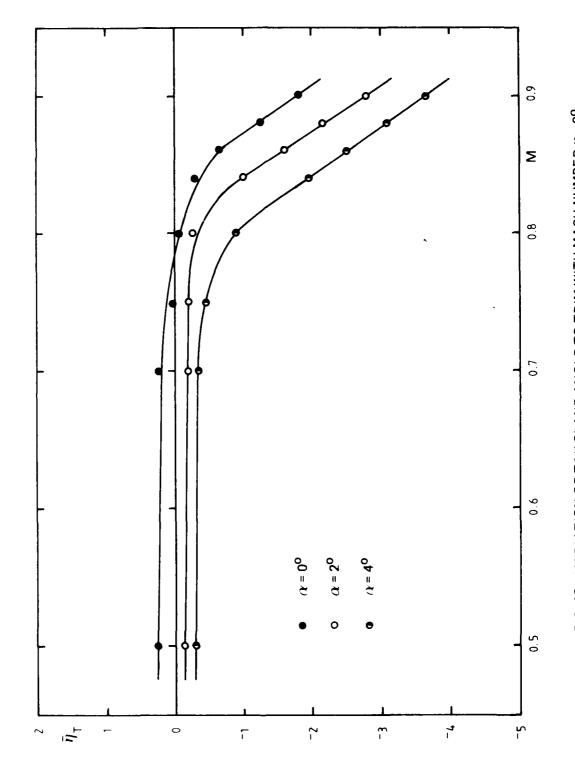


FIG. 13 VARIATION OF TAILPLANE ANGLE TO TRIM WITH MACH NUMBER η = $0^{
m O}$

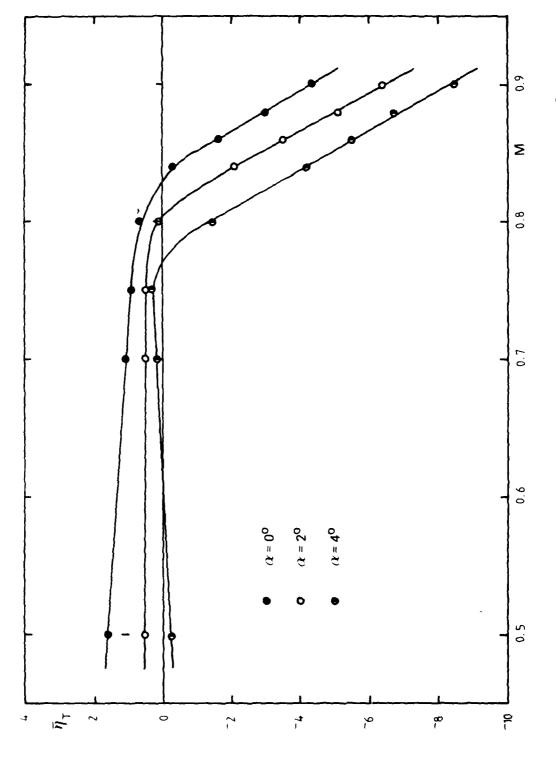


FIG. 14 VARIATION OF ELEVATOR ANGLE TO TRIM WITH MACH NUMBER $\eta_{
m T}$ = $\%^{
m O}$

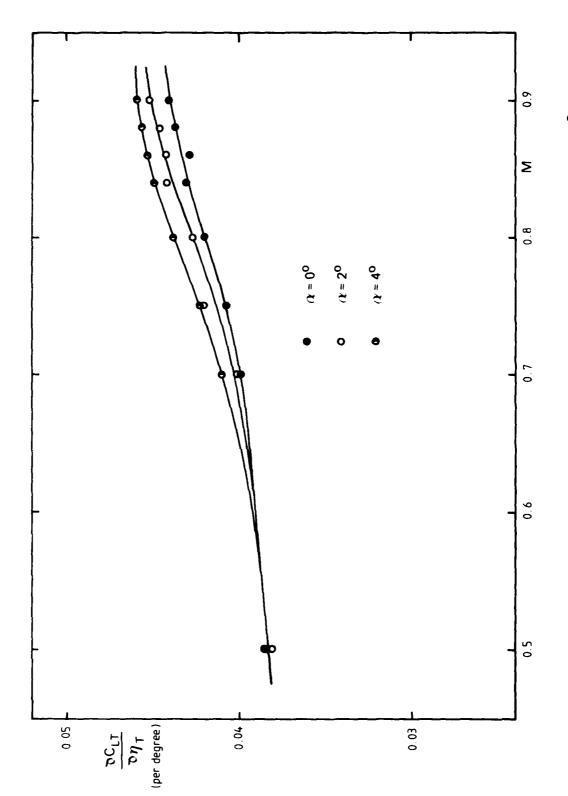


FIG. 15 VARIATION OF TAILPLANE EFFECTIVENESS WITH MACH NUMBER η = $0^{
m o}$

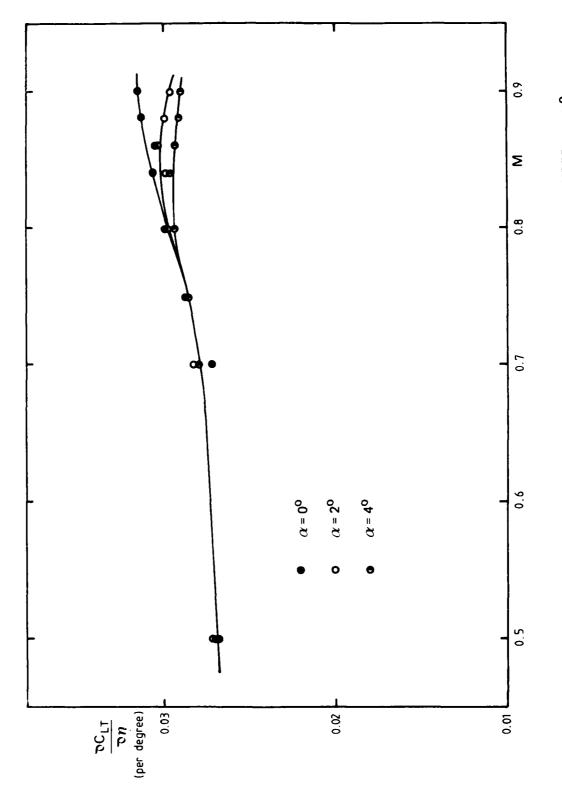


FIG. 16 VARIATION OF ELEVATOR EFFECTIVENESS WITH MACH NUMBER $\eta_{\rm T}$ = $\%^{
m O}$

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